COLOUR TV SERVICE MANUAL



Issue 1 August 1984

Main Chassis Information

(including preset adjustments, alignment and circuit description)

PC1150

For Service Manuals Contact
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The TX100 chassis is an advanced technology product catering for a wide range of models and facilities. By varying the component make up, the single board chassis is capable of driving various sizes of 90° and 110° picture tubes.

High levels of safety, reliability and ease of servicing have been attained with the TX100 chassis. Apart from a small area which is protected by safety covers, the chassis is fully isolated from the mains, thus permitting the addition of peripheral facilities without further isolation. Reliability is improved by a lower component count, a large number of which are automatically inserted employing the latest production

techniques. Servicing is made easier by a reduction in the number of preset adjustments and simplified test procedures, for example auto black level setting is provided by the luma/chroma IC, thus removing the presets from the video drive stages.

The TX100 chassis will accept additional modules for remote control, teletext, baseband stereo sound and other facilities to be included in certain models. The chassis is extendable for RF stereo sound should a suitable system be launched by the broadcasting authorities. By adding a small printed circuit board the chassis will accept Peri television input/output facilities. Connecting pins for most of the facilities are already provided.

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CONCISE SPECIFICATION

The specifications for remote control, teletext etc., are given in the relevant sections of this manual.

POWER SUPPLIES

Nominal: 240V a.c. 50Hz. The chassis is fully mains isolated and is stabilized across mains voltage range 185V to 265V for less than 0.75% change in picture size. No mains input adjustment is required.

POWER CONSUMPTION

240V a.c. supply

90° Tube: Typ

Typically 65W with normal picture; 80W at 1mA beam current; 55W at zero beam

current.

110° Tube: (30AX) Typically 80W with normal picture; 90W at 1mA beam current; 68W at zero beam

current.

FREQUENCY COVERAGE

UHF channels 21-68

471 · 25MHz-847 · 25MHz (vision carriers)

TUNER

Electronic varicap with voltage stabilization and AFC.

SENS!TIVITY

 $30\mu V$ p.d. into 75Ω (60 μV emf) with a locked colour picture.

MAXIMUM SIGNAL INPUT

Any channel 20mV at aerial input for 1% cross-modulation.

VISION IF

Adjacent channel (vision) 31.5MHz. Sound carrier 33.5MHz. Chroma sub-carrier 35.07MHz. Vision carrier 39.5MHz. Adjacent channel (sound) 41.5MHz.

AUDIO OUTPUT

2.7W rms into 16Ω at less than 5% THD

PICTURE TUBES

90° Type:

In-line with integral saddle/ toroidal self-convergence

deflection yoke.

110° Type: (30AX) In-line with integral saddle/ saddle self-convergence

deflection yoke.

110° Type: (S4) In-line with integral saddle/ toroidal self-convergence

deflection yoke.

BEAM CURRENT LIMITING

1mA ±10%

EHT

Zero beam current: 25kV maximum for 90° tube (26-5kV for 110° tube).

1mA beam current: 22.7kV for 90° tube (24kV for 110° tube).

The above figures are subject to ± 0.7 kV tolerance.

INSTALLATION

Mains Connection

The receiver operates from a.c. mains supplies 185V-265V 50Hz. No input adjustment is required.

The chassis is isolated. As indicated on the top printing, an area of the printed circuit board carries live mains and this is protected above and below by plastic covers which should not be removed unless absolutely necessary.

Fuse

FS1 mains input T1A6 (20mm cartridge type).

Degaussing

The built-in degaussing circuit operates whenever the receiver is switched on from cold, neutralizing all but the most severe cases of magnetization.

On installation, the receiver may be manually degaussed with an external coil should this be considered necessary.

Aerial

A wide bandwidth aerial is required and careful siting and orientation are necessary for the best signal strength with freedom from ghosting on all available channels. This is particularly important when installing a receiver fitted with teletext facilities. Low-loss 75Ω coaxial feeder should be used.

Varicap Tuning

The location of the tuning potentiometers and the method of defeating the AFC depends on the particular model. However, in most cases the AFC is automatically defeated whilst gaining access to the tuning potentiometers.

Switch on and select the desired programme number. Ensure that the AFC has been defeated and operate the tuning potentiometers to obtain the required station. Tune to between loss of colour and patterning. Finally check that no change to tuning occurs with the AFC on or off and readjust if necessary to achieve this.

ACCESS FOR SERVICE

Removing Cabinet Back

The cabinet back moulding hooks into slots in the cabinet base, and is held at the top by either plastic screws or by a simpler fixing using a barb and catch arrangement. The catch is released by inserting a screwdriver into the slot provided, and pushing down on the barb whilst pulling the back away from the cabinet at the top. Swing back the top to free the moulding from the slots in the cabinet base.

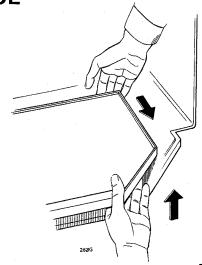
Chassis Removal

The chassis frame is positioned in the bottom of the cabinet by lugs on either side of the frame which locate in slots at the bottom of the cabinet. The chassis is latched into the cabinet base by a lip on each of the rear lugs.

To remove the chassis, lift the right-hand side rear of the chassis frame in order to delatch it. With the other hand, push the right-hand side front of the chassis frame towards the rear of the cabinet; refer to diagram. Repeat this procedure with the left-hand side of the chassis frame after which the chassis may be removed or fitted into the servicing position.

Chassis Servicing Position

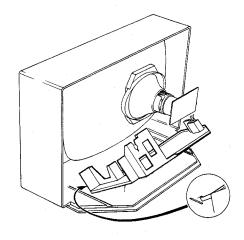
The chassis may be fitted into a sloping position to enable the printed circuit board to be easily serviced whilst in an operational mode, both component and copper sides being accessible. The two protruding lugs at the front of the chassis frame slot into the cabinet base. Two positions are available; refer to diagram.

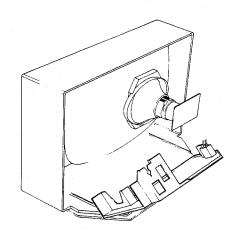


SAFETY COVERS

Moulded plastic covers, one above and one underneath the printed circuit panel, give protection over the live mains area of the chassis. If removed for servicing, adequate precautions must be taken until they are replaced.

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SERVICING NOTES

Removal of Components. To avoid damage to the copper track when removing components, it is advisable to use a solder wick and not a solder sucker. In addition, it should be noted that many components have been automatically inserted into the printed boards and this process involves bending of the leads underboard prior to soldering. Therefore to remove these components it is recommended that their leads be cut above the board and the soldered remains removed from below.

Replacing chopper and line output transistors TR6 and TR10. These transistors are mounted on heatsinks. The transistors are secured to the heatsinks by spring clips. To remove the clip, simply press it out from the inside of the heatsink. It is not necessary to remove the heatsink from the PCB.

Before replacing the transistors, inspect the insulating washers and replace if necessary. Secure the transistors to the heatsink by pressing the spring clip firmly in position.

Replacing ICs Mounted on Heatsinks. In the majority of cases, when replacing the ICs that are mounted on heatsinks, it is easier to remove both the heatsink and IC from the PCB, then remove the IC from the heatsink. Before replacing the IC, clean off the old heatsink compound from the heatsink and insulating washer (if fitted), and apply fresh compound to both sides. Always ensure the IC retaining screw is secured tightly.

Integrated Circuits. All ICs are vulnerable to static damage unless properly mounted in printed circuit boards or in approved packing.

They must be handled with care and must not be loosened, removed from or inserted into a live circuit.

Touch an earthed object before handling any IC or PCB and use an earthed soldering iron.

Replacement ICs are specially packed in conductive material, which may be plastic.

Keep ICs in transit packing until used and when returning suspect devices under guarantee, always protect them in the original packing.

Do not use non-conductive plastic such as polystyrene even for temporary storage of ICs.

SERVICING ADJUSTMENTS

The following preset adjustment procedures are not required during installation and should be made, only if necessary, after servicing.

WARNING

EHT Shock Hazard

The EHT must be safely discharged before attempting to disconnect the EHT lead from the tube anode.

Clip one end of a convenient lead, such as a meter lead, to the tube earthing strap on the tube body, fold back the suction cap and discharge the EHT through the lead.

Press in one side of the spring clip which projects into the tube cavity to ease removal of the EHT connector.

IMPORTANT

Do not disturb the tube neck adjustments as these have been set for optimum performance during tube manufacture.

Before attempting the following adjustments the receiver should be tuned if possible to a test card with the brightness, contrast and colour controls adjusted for the best picture, unless stated otherwise.

Receivers fitted with remote facilities should be normalized by switching off and on again before adjusting the preset controls. On certain receivers some of the analogue controls, i.e., brightness, contrast etc., may be presets on the remote control receiver board.

The adjustments should be carried out in the following order for convenience.

Set HT (RV13)

Turn contrast and brightness controls to minimum for zero beam current. Check voltage at pin 5 of LOPT with a $20k\Omega/volt$ meter of 2% accuracy. If necessary, adjust RV13 for 119V (90° tube) or 148V (110° tube). Adjust contrast and brightness for best picture.

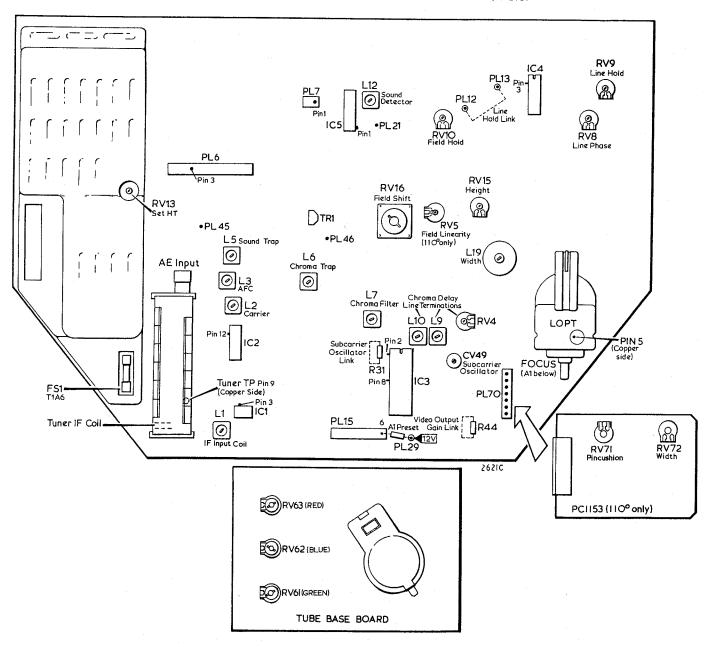
Picture Geometry

Line Hold (RV9)

Link PL12 and PL13 together. Adjust RV9 for the best floating but resolved display attainable. The display will lock when the link is removed.

Field Hold (RV10)

RV10 is a factory preset adjustment which is set for 46Hz free running at pin 3 of IC4 with sync removed by linking PL12 to PL13.



DVM Method

Turn RV10 fully counter-clockwise. Turn RV10 clockwise until field just locks; measure volts on pin 3 of IC4. Continue turning RV10 clockwise until lock is just lost; again measure volts on pin 3 of IC4. The approximate position of RV10 is halfway between the two voltage measurements taken.

Alternatively

If a DVM or oscilloscope is not available, adjust as follows:-

Starting with RV10 fully counterclockwise, adjust for a steady picture and note the positition. Continue rotation until the picture suddenly increases in height. Then back off until approximately half way between these two positions.

Pincushion (RV71-110° only)

Adjust RV71 for straight verticals at the edges of the display.

Field Linearity (RV5-110° only)

Adjust RV5 for best field linearity at the top and bottom of the display.

Line linearity is fixed.

Picture Shift (RV8 and RV16)

Adjust Line Phase RV8, and Field Shift RV16 to centre the display.

Picture Size (L19, RV72 and RV15)

Adjust Height control RV15 in conjunction with Width control L19 for

90° or RV72 for 110°, for full scan consistent with a correctly proportioned display.

Focus

Adjust for optimum overall resolution.

A1 Preset

Ensure that the A1 preset is at mid position.

Blank out the picture by connecting PL15 pin 6 to PL29 (12V) via a $1\cdot 5k\Omega$ resistor. Connect the oscilloscope locked to frame rate, to the tab of one of the video output transistors TR61, TR63 or TR65.

Referring to the diagram, measure Vo for each of the video outputs and note which one has the highest value.

Adjust the A1 preset to make the highest value of Vo noted equal 150V.
Remove the oscilloscope and shorting

Va

Alternatively:

With a normal picture displayed, ensure that the A1 preset is at mid position. Rotate the A1 preset clockwise until the picture begins to lose contrast and note the position of the screwdriver slot.

Rotate the A1 preset counter-clockwise until the picture again begins to lose contrast or loses one colour, and note the position of the screwdriver-slot. The

approximate position of the A1 preset should be midway between the two noted positions of the screwdriver slot.

Grey Scaling Procedure

Video Output Gain (RV61, RV62 and RV63)

The video output gain presets RV61, RV62 and RV63 should be at about midposition before grey scaling.

Disable the beam limiter by connecting a shorting link across R44.

Turn the contrast control to maximum and the brightness control to a little less than mid position.

Connect the oscilloscope to the tab of one of the video output transistors and adjust the appropriate gain preset for 100V black to white. Repeat for the other two colours and then remove the shorting link across R44.

Alternatively:

Ensure that the three video output gain presets RV61, RV62 and RV63 are set to mid position.

Highlights Final Adjustment

With a suitable picture displayed inspect the highlights for colouration.

If green, turn down RV61.

If red, turn down RV63.

IMPORTANT:Do not readjust the blue output gain preset RV62. If highlights are blue, turn up red and green presets.

CIRCUIT ALIGNMENT

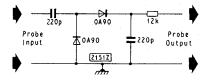
Unless it is known that a panel is misaligned or that tuning components have been replaced, all other causes for a particular fault condition should be checked before realignment is considered. Receivers fitted with remote control facilities should be 'normalized' by switching off and on before proceeding.

Equipment Required

Where appropriate, an alternative method of adjustment is given to cover situations where suitable test equipment is not available.

- 1 An IF wobbulator with markers.
- 2 An AM signal generator with an output impedance of approximately 75Ω , and with an accurate frequency calibration covering a range of at least 1MHz to 45MHz.
- 3 An FM signal generator with an output impedance of approximately 75Ω , and with an accurate frequency calibration covering the range 4MHz to 6MHz.
- 4 An oscilloscope capable of displaying 100mV at 6MHz.
- 5 A multirange meter ($20k\Omega/V$) such as the AVOmeter Model 8.
- 6 Non-metallic trimming tools and a suitable tool for adjusting sub-minature potentiometers.

- 7 A $100k\Omega$ linear potentiometer and a 10nF capacitor.
- 8 A detector probe such as the one shown below.



Preliminaries

Test connections can be soldered to the copper side of the printed circuit board (with the receiver switched off); lead lengths should be kept to a minimum.

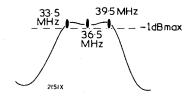
Tuner Output and Vision IF

Tuner IF Output Coil and Input Coil (L1) Bandpass

Wobbulator Method

Connect the output lead from the wobbulator (terminated with 75Ω) between pin 9 of the tuner and earth. Connect the input of the detector probe to pin 4 of IC1 with the earth wire soldered to L1 can. Connect the probe output to the oscilloscope. Link PL45 to earth in order to mute the detector IC (IC2).

Set the wobbulator centre frequency to 36.5MHz and the output to maximum, and switch on the receiver. Adjust the wobbulator 'Y' gain to give a full scale display. Switch on markers at 39.5MHz and 33.5MHz. Adjust the tuner IF output coil and the input coil (L1) bandpass for a symmetrical response centred on



The markers should be no more than 1dB down the slope. No further adjustments are necessary.

Spot Frequency Method

Connect the output of the signal generator between pin 9 of the tuner and earth. Link PL45 to earth and connect the detector probe between pin 3 of IC1 and earth as for the wobbulator method. Feed the detector probe output into the oscilloscope 'Y' amplifier, set to d.c.

Set the signal generator to 38.9MHz. Turn up the generator output and adjust the oscilloscope 'Y' amplifier gain for a satisfactory indication (shift of trace). Remove L1 input coil core and adjust the tuner IF coil for maximum output at 38.9MHz. Insert L1 input coil core. Set the signal generator to 35MHz and tune L1 for maximum output. (Note: L1 has two peaks, the correct tuning position is with the core below the former and can top). Without removing the core repeat the two adjustments as necessary to ensure the output at these two frequencies is the same. Switch off the receiver and disconnect the generator, probe and earth link.

Continued . .

Carrier (L2) and AFC (L3) Coils

To set these coils an accurate signal source is essential. Connect the terminated signal generator between pin 9 of the tuner and earth and set the frequency to 39-5MHz. Connect a $100k\Omega$ linear potentiometer connected as a variable resistance between PL45 and earth. Connect a meter set to d.c. between PL46 and earth.

Switch on the receiver, and with zero output from the generator, adjust the potentiometer until noise just disappears from the TV screen. Then increase the output from the generator until the d.c. level drops down below the nominal zero output 6V level. Adjust L2 for maximum output at the carrier frequency (minimum voltage reading) and adjust the generator to make the reading approximately 4V d.c.

With the same signal input, remove the potentiometer and using a digital voltmeter or AVOmeter (25V range) adjust L3 until the voltage on pin 3 of PL6 is the nominal 6V level.

Switch off the receiver and disconnect the generator and meter.

Sound IF

6MHz Sound Trap (L5)

Spot Frequency Method

Switch off receiver.

Link PL45 to earth.

Connect the generator (terminated with 75 Ω and d.c. isolated with 10nF) between IC2 pin 12 and earth. Connect the oscilloscope between the base of TR1 and earth.

Switch on the receiver. Set the signal generator to full output and the frequency to 6MHz CW. Tune L5 for minimum deflection at 6MHz on the oscilloscope screen.

Remove oscilloscope, generator and earth link.

Alternatively:

Operate the receiver with a colour signal applied to the aerial input (standard colour bars if available). Connect the oscilloscope between PL46 and earth.

Set L5 core flush with the top of can and then turn downwards through loss of colour until colour is restored. Then adjust for minimum sound-chroma beat on the TV display (corresponding to minimum 6MHz on the oscilloscope).

Sound Detector (L12)

If it is suspected that the Vision IF alignment has been disturbed, the latter should be checked before adjusting L12.

FM Signal Generator Method

Switch off the receiver and link PL45 to earth.

Connect the FM signal generator (terminated with 75 Ω and d.c. isolated with 10nF.) between IC2 pin 12 and earth.

Connect the oscilloscope set to 0.5V/cm sensitivity between PL21 and earth.

Set the generator frequency to 6MHz 50kHz deviation, level about 10mV. With the receiver switched on, adjust L12 for maximum symmetrical sine wave display on the oscilloscope. Pin 3 of IC5 is independent of the volume control setting. At maximum volume the sound just clips at around the 2·7W level on PL7/1.

The ceramic filter CF1 is non-adjustable. If it is required to check its response, keep the signal generator connected as above, switch to CW, and connect the oscilloscope probe between pin 1 of IC5 and earth.

Adjust the output level of the generator in conjunction with the 'Y' gain of the oscilloscope until a measurable waveform is displayed. Now swing the generator frequency slowly from 5-9MHz to 6-1MHz and check that the amplitude of the waveform does not change by more than about 6dB.

Alternatively:

Plug in an aerial feed and tune to a suitable signal. Coarsely tune L12 so that the programme sound is heard and then adjust L12 for minimum video buzz and maximum recovered sound.

4 · 43MHz Chroma Trap (L6)

With an off-air colour signal applied to the aerial input (standard colour bars if available), and the oscilloscope probe connected to the junction of C27-R22-R23, adjust L6 for minimum burst.

Alternatively:

Adjust L6 for minimum chroma patterning on the picture with the colour control at minimum.

Chroma Input Filter (L7)

Spot Frequency Method

Switch off receiver.

Link PL45 to earth.

Connect the generator (terminated with 75 Ω and d.c. isolated with 10nF) between PL46 and earth. Connect the oscilloscope via a 10pF capacitor, between the junction of C29, C30, R24 and R26 and earth.

Switch on receiver.

Set the signal generator to 4·43MHz. Tune L7 for maximum peak at 4·43MHz on oscilloscope screen.

Remove the generator, oscilloscope and earth link.

Alternatively:

Measure the d.c. volts on pin 2 of IC3. Display a locked colour picture and adjust L7 for maximum d.c.

NOTE: The meter must not load pin 2 appreciably.

Chrominance Adjustments

The following setting up instructions are carried out with the receiver operated from an off-air colour bar signal or UHF colour bar generator connected to the aerial socket.

Set the customer controls as follows: brightness to the centre of its range, contrast and colour to approximately two-thirds of their maximum setting.

Subcarrier Oscillator (CV49)

Short circuit R31 in order to override the colour killer and colour control. Whilst looking at a colour picture, attenuate the aerial signal. Using a non-metallic trimming tool, adjust the trimmer CV49 to achieve colour lock on the weakest signal possible, occasionally interrupting the signal in order to indicate correct colour pull-in.

Reconnect the aerial and disconnect the short circuit.

Alternatively:

Short circuit R31 and link pins 24 and 25 of IC3 together. Using a non-metallic trimming tool adjust CV49 for zero frequency run through. Remove the links.

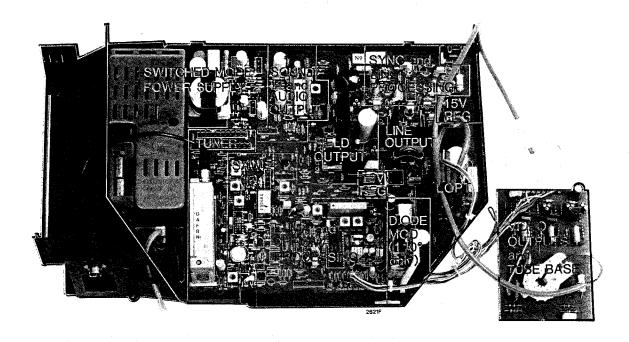
Chroma Delay Line Terminations (RV4, L9 and L10)

Set L10 core one and a half turns down from the top of the former and adjust RV4 and L9 for minimum venetian blind effect. In a very few cases balance may be unattainable by adjustment of L9. If so, adjust L9 for the best setting and trim L10 for balance.

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Circuit Description

MAIN CHASSIS (PC1150)



General Indication of Circuit Locations

GENERAL

The isolated power supply is a switched mode type using a TDA4600-2 (IC7) as the control IC, with a T9063V (TR6) chopper transistor. To eliminate the need for a separate standby transformer in remote control models, a relay, RL1 is fitted. This is de-energised during standby to break the main HT supply (119V).

The electronic varicap tuner is band-pass coupled to the SL1432 (IC1) preamplifier which drives a SW153 (SF1) SAW filter. The main IF gain detector, AFC and AGC circuits, are contained within the TDA3540 (IC2).

The complete sound stage IF and audio is within a single TDA1701 (IC5).

A TDA3562A (IC3) performs luma/ chroma processing as well as providing direct input for digital signals with fast blanking ability, together with auto black level setting. Wide band class A video output stages are mounted on the tube base PCB, the only adjustments being for the gain controls to set correct white level.

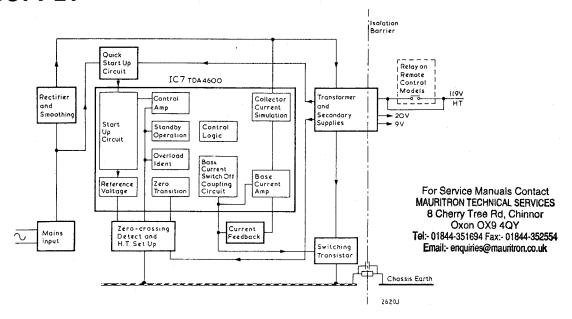
The video signal from the IF is taken through filters to the TDA2578A (IC4). In addition to performing all the synchronization, IC4 also provides 50Hz/60Hz detection and height adjustment, and a video transmitter ident circuit for sound mute when no sync is present.

IC6, which contains the whole field stage, differs between the 90° tube and the 110° tube versions. The heatsink and a number of components change value but the basic circuit is common. The only adjustments are for height and d.c. field shift. An output from IC6 is used by the TDA2578A (IC4) to sense field timebase operation and blank the CRT in the event of the timebase failing.

The line drive from IC4 is used to drive the line timebase via a low voltage transistor and driver transformer circuit, feeding a diode-split line output transformer. The LOPT provides EHT, focus and A1 volts, tube heater supply, and the mains low voltage supply of 12V via an IC regulator. The circuit differs between the 90° tube and the 110° tube versions. The 90° version is designed to drive pincushion distortion free tubes and has no diode modulator. The width control is by a variable inductor. The 110° version boosts the basic 119V power rail and has a plug-in diode modulator PCB to provide E-W raster correction and width control. The LOPT (T3) differs between the 90° tube and the 110° tube versions of the receiver.

The circuit description which follows is for both the 90° tube and 110° tube versions of the basic chassis, and is not specific to any one particular model.

POWER SUPPLY



The isolated power supply is a switched mode configuration; IC7 being the control IC and TR6 the chopper transistor. At zero beam current the main HT rail for 90° tube receivers is 119V, set by RV13. RV13 is adjusted to give 148V as the boost rail on 110° tube receivers. There are two LT supply rails; one for 20V and one for 9V.

The mains input is fed via the bridge rectifier circuit D5-D8 and smoothing capacitor C110, to the chopper transformer T1. Switch-on current limiting resistor R106 also supplies the silicon controlled rectifier (SCR) quick start circuit. SCR1 anode is fed via R116, and the gate is fired from the a.c. supply via R117 and R118.

During the positive half-cycle SCR1 switches on, charges up C119 and supplies start-up current to pin 9 of IC7. The start-up is thus set by the R116/C119 time constant. Once IC7 is activated, a supply of nominally 12V is fed from T1 via D12, to pin 9 of IC7. This voltage is higher than that supplied via SCR1 and is thus higher than the SCR gate voltage which is set by D11. D10 is therefore

forward biased and the SCR gate is driven negative with respect to its cathode. On the next a.c. negative halfcycle, SCR1 turns off.

IC7 has its own start-up sequence to ensure correct switching of the chopper transistor TR6 from the first cycle of operation. The sequence is as follows:

The start-up enables the coupling capacitor C117 charging circuit, and an internal reference of 4V is built up. The current drawn from the supply is approximately 3mA.

This internal reference voltage is switched to all sections of the IC when the input voltage from D12 reaches its normal 12V.

The control logic is then enabled and drive to the chopper transistor TR6 commences. Should the voltage at pin 9 of IC7 drop below 7V, the control logic will be blocked and the base current amplifier drive will be disabled.

A facsimile of the collector current flowing in TR6 is provided by R115 and C118 at pin 4 of IC7. C118 is allowed to charge up whilst the transistor is on and is discharged when the transistor is switched off. The sawtooth-shaped rise at pin 4 of the IC is impressed on the base current amplifier within the IC, and is used to drive the switching transistor via pins 7 and 8, providing a base current proportional to the collector current. The sawtooth waveform also provides current limit information. D14 and R134 are incorporated in the circuit to reduce the rate of discharge of C120, thus assisting the transistor operation. This is especially useful during standby.

On receivers fitted with remote control, the chopper supply is left operative in the standby condition so that the remote circuit can be powered from the receiver 20V supply line. A relay is used to disconnect the main HT rail, thus preventing the rest of the circuitry of the main chassis from operating. In this state, the operational frequency of IC7 increases to 60kHz due to the reduction of loading. R122 provides a minimum loading in the standby state so as to ensure that IC7 remains within its operating curve. The 9V rail is mainly used to power teletext circuitry and TR7 disconnects this rail in the standby mode.

TUNER AND IF

The SC4 Mark III tuner output drives the IF preamplifier IC1, via bandpass coil L1. The preamplifier provides not only the necessary gain block between the tuner and Surface Acoustic Wave Filter (SAWF) SF1, but also supplies a broad band AGC signal to the tuner via R14, the level being preset by R8 and an internal resistor chain, to maintain conditions equal to a 1.5mV signal input at the aerial socket.

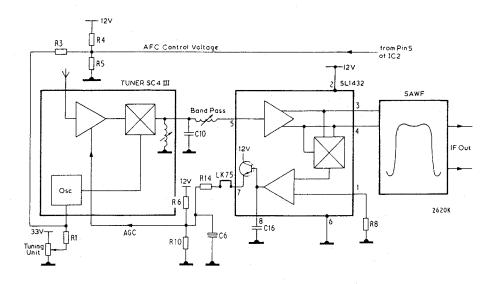
The main chassis is multi pierced for a standard 'T08' SAWF and also for a parallel sound SAWF. The output from the SAWF is fed to the IC2.

IC2 consists of an AGC controlled IF amplifier which has an overall gain of 60dB resulting in a sensitivity of only $60\mu V$ for the onset of IF AGC. The AGC has a control range of 64dB.

The AGC detector compares the top of synchronisation with an internal 3V reference. Any deviation from 3V

changes the charge on the storage capacitor C22, at pin 14. This change, reflected at pin 3, is smoothed by C18 and applied to the internal IF amplifier block.

If a negative going noise spike causes the video output to reduce to below 1·8V, a noise gating circuit generates two outputs. One reduces the current from the AGC detector so as to minimise any spurious AGC action, whilst the other is



applied to the noise inverter where it causes the video to be clamped at 3.8V for the duration of the noise spike.

The synchronous demodulator is a type in which the video modulated IF is multiplied by its own carrier, giving an exact replica of the original video with little, or no, non-linear or quadrature distortion. The output signal is also free of odd harmonics.

The reference amplifier is tuned by L2 and C23. Since the internal collector circuits cause very little clamping, the tuned circuit has a very high loaded Ω . Internal diodes are fitted in parallel with the circuit, thus limiting the amplitude of the reference signal and avoiding radiation problems.

Since any mistuning will produce phase errors, the AFC circuit has a double balanced comparator with a portion of the reference signal being a.c. coupled. The required capacitance is very low and

is actually formed by inter-track capacitance on the PCB. The other input being fed by L3 and C25. If the two signals are in quadrature, the AFC demodulator does not generate any output. Any frequency deviation of the IF carrier causes a phase difference between the two inputs, thus causing a proportional change of current at pin 5 of the IC. This variation is converted to a delta voltage at pin 5 of the tuner by R3, Z1 and R1 and the tuner unit. The AFC is defeated by taking IC2 pin 6 below 1 · 6V, which reduces the current at pin 5 of the IC to zero.

Because of the asymmetric noise spectrum, due to the Nyquist slope, C26 and R52 are added to make the noise symmetrical, as seen by the AFC circuit.

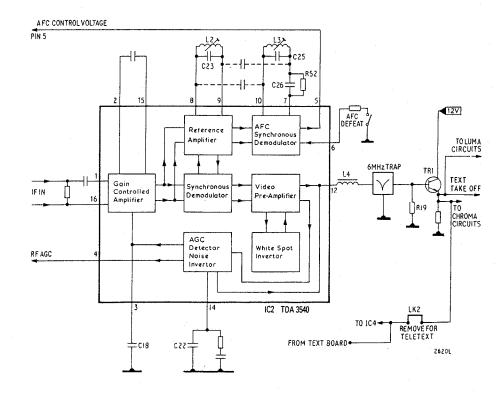
The video output is protected from interference by a white spot inverter and if any noise pulse with an amplitude

greater than 6.8V is received, the video output is clamped to 4.7V for the duration of the pulse.

The video feed to emitter follower TR1 base is via choke L4 and 6MHz bridge-T sound trap L5 and associated components. L4 reduces capacitance loading on the output so that any residual harmonics are kept to a minimum. R19 is incorporated to damp the quadratic factor of the trap so that the video response is flat to 5.2MHz.

When teletext is incorporated, take-off is via PL19 pin 5 which incorporates the required insertion for After Hours Synchronisation (AHS). The emitter follower TR1, is included to ensure optimum text performance.

The fact that a parallel sound SAWF can be accommodated has already been mentioned and the PCB is also pierced for parallel sound using a TDA 2525 and a buffer, so that the sound IF may be supplied to standard stereo processing circuits.



2

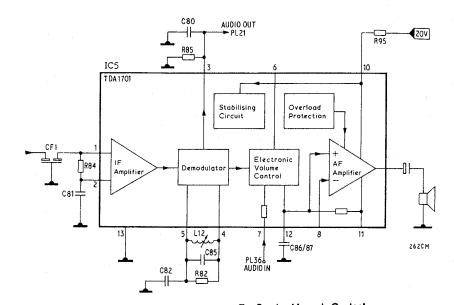
SOUND IF AND AUDIO

The special heatsink for IC5 enables the IC to develop 2.7W RMS audio power into 16 ohm loudspeakers.

The 20V supply feed is applied to pin 10 of IC5 via safety resistor R95. Composite video plus intercarrier sound, is fed direct from the vision IC2 to the ceramic filter CF1. The output of the filter is connected to the input of IC5. PL35, on pin 2 of IC5, is provided for a sound IF input muting connection when the IC is fed from an external audio source via PL36.

By adjustment of RV11, the volume is controlled electronically by varying the d.c. voltage feed to pin 6. Tone controls, when fitted, are connected via PL16. If treble and bass controls are fitted, LK3 and C86 are removed. R91 and C93 are incorporated to ensure stability under all conditions by providing the necessary phase shift. An audio output, unaffected by the receiver volume control, is provided at PL21.

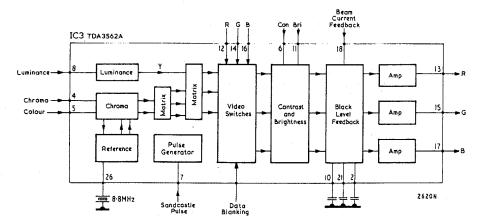
IC5 contains internal overheating protection; when it reaches a temperature of 150°C, the output stage shuts down until the temperature decreases.



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VIDEO/CHROMA PROCESSING AND VIDEO OUTPUT



In addition to providing luma/chroma processing, IC3 eliminates the need for the three background adjustment controls as an automatic beam current adjusting system is incorporated within the IC. Another feature of IC3 is that the inserted RGB signals are contrast controlled.

Luminance

After passing through the delay line DL2, the luma signal is applied to IC3 at pin 8. Before being passed to the matrix circuits, the luminance component is black level clamped and an artificial black level is then added. Contrast and brightness control is carried out after the matrixing process.

Chrominance

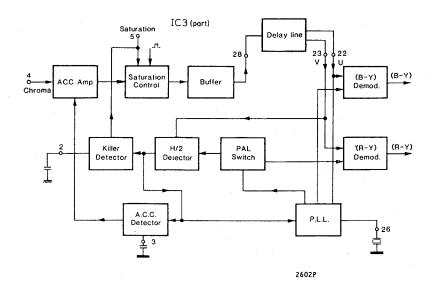
After filtering out the chroma signal from the composite video, it is applied to pin 4 of IC3. After ACC and amplification processing, the chroma signal leaves via pin 28 and passes through the chroma delay line DL1.

Up to this point the chroma signal amplitude has been affected by adjustment of the colour control but because the chroma delay line is inside the ACC loop the amplitude of the burst remains unaffected by the colour control as the burst amplitude is maintained at a constant level by the ACC loop.

The chroma delay line separates the chroma into its U and V components

which are then returned to IC3 via pins 22 and 23 respectively. Subcarrier phase control is achieved by reference to the U signal. The crystal oscillator is a one-pin-configuration, connected to pin 26. The oscillator operates at twice subcarrier frequency in order that the 90° phase shift necessary between the U and V references can be achieved digitally, that is, without external components. Ident, ACC and colour killing are achieved conventionally by using the subcarrier phase control error signal.

After demodulation, the R-Y and B-Y are matrixed to give the G-Y, and these three signals are then applied to the RGB matrix block where luminance is added.



Video Amplifiers

Once the RGB signals have been produced, an internal switch selects either these internal RGB signals or external signal data applied to pins 12, 14 and 16. The choice is governed by the voltage applied to pin 9; 0V for internal, 1V for external data. The selected signals are then contrast and brightness controlled after which they are amplified and finally passed through black level feedback clamping circuits, leaving IC3 on pins 13, 15 and 17.

Automatic Black Level Adjustment

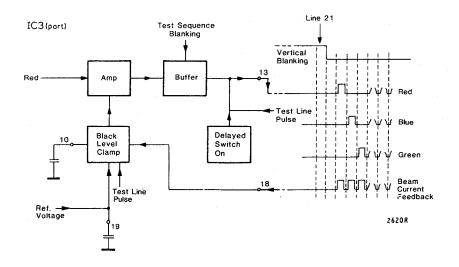
This system, also known as automatic CRT cut-off, replaces the background adjustments that are found in conventional receivers. Since each gun will require a different cathode voltage for cut-off, this system automatically sets these voltages. It achieves this by sending out a test line and adjusting the cathode voltage to produce a beam current of approximately 10µA for the duration of the test line. Cut-off is

therefore, not absolute. Although very faint, $10\mu A$ beam current is nevertheless visible, and the test lines are therefore inserted at the top of the picture during lines 23, 24 and 25. These lines are produced in IC3 by first blanking the video and then inserting a pulse during line 23 for the red gun, line 24 for the blue and line 25 for the green. This portion of the picture is normally lost due to overscan.

Beam current control is therefore carried out sequentially with the video output circuit arranged to detect beam current. During the test lines, pin 18 of the IC3 changes state internally. The video amplifiers provide approximately 5 volts to pin 18, this being proportional to the beam current. Should this voltage be outside the predetermined limits, the feedback amplifiers inside IC3 modify the output voltage until the result is inside the limit. The error signals are then stored on external capacitors C45, C50 and C51, so that the state remains constant until the next set of test lines one frame later.

After switching on, the CRT takes time to warm up. Under the arrangement just described, the $10\mu A$ would initially be missing. IC3 would sense that the CRT was not being driven hard enough and would adjust the cathode voltages, effectively to peak white. As the CRT warmed up, the effect would be that of a peak white raster slowly drifting down to a normal picture as the automatic system took control. To avoid this undesirable state of affairs, a special start-up sequence is used.

Immediately after switch on, IC3 transmits a series of test lines, approximately 20 per field. As soon as beam current is detected, the test lines are switched off and an internal timer is enabled. The picture is blanked for the duration of the timer; four seconds approx., during which time the warm up of the CRT is completed. When the timer sequence ends, normal operation is resumed and the picture information is released to the CRT.



VIDEO OUTPUT AMPLIFIERS

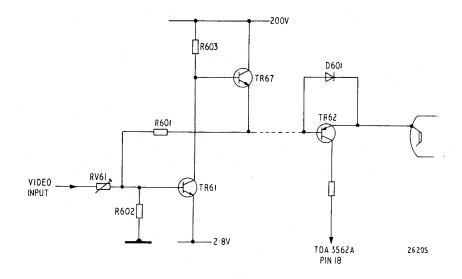
The video output amplifiers are fitted on the tube base PCB.

Since the three amplifiers are identical, reference will be made to the green channel for description purposes.

Amplifier TR61, with high value load resistor R603, is assisted by emitter follower TR67. The gain is stabilised by feedback through resistor R601 and set by the ratio R601:RV61 to about 20.

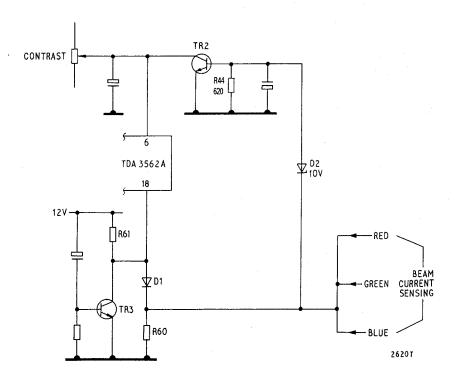
TR62 senses the beam current. Under steady state conditions, beam current flows out of the CRT cathode, through TR62 and thence to the network connected to pin 18 of IC3. Under dynamic conditions, the cathode voltage is raised by current flowing through TR67 and D601 into the cathode capacitance. The cathode voltage is lowered by current flowing out of the cathode capacitance through TR62. This current is controlled by the voltage on the base of TR62. It can be seen, therefore, that when charging up the cathode capacitance, TR62 is reverse biased, thus beam current cannot be sensed.

The video amplifiers have a swing of 100V from black level to peak white.



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BEAM CURRENT LIMITING

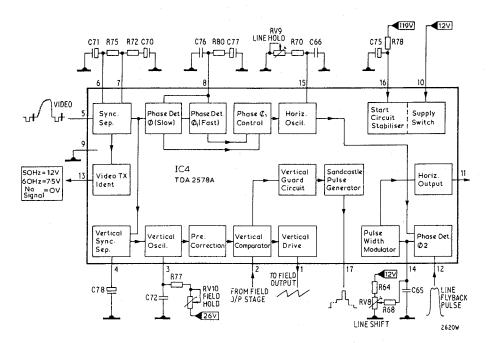


Beam current is presented to pin 18 of IC3 via diode D1. During switch-on there are many stray currents associated with rising supply lines which could confuse the logic on pin 18. To prevent this, pin 18 is shorted to ground by TR3 for the first 1.5 seconds after switch on. Beyond this time, TR3 plays no part and can be considered as open circuit.

For most of the frame period, pin 18 of IC3 is isolated from the beam current by D1. Total beam current from the CRT cathodes pass through R60 producing a voltage across it. When this voltage exceeds 10V, D2 is turned on and the beam current flow is through D2 and R44. The voltage developed across R44 finally turns TR2 on and pulls the contrast control voltage down. This in turn, reduces the beam current, and the loop is completed. Beam current limits at approximately 1mA.

When the test lines, to which reference has previously been made, are transmitted for the automatic black level system, pin 18 of IC3 is switched on internally. $10\mu A$ of beam current then flows into the network R61, D1 and R60 generating about 5V, this then stabilises the background loop. 5 volts is insufficient to turn on D2 and the beam limiter circuitry is therefore disconnected.

SYNC PROCESSING, LINE AND FIELD OSCILLATORS



IC4 combines the functions of a noise gated sync separator, line and field oscillator and sandcastle pulse generator. It takes the composite TV signal and extracts the vertical and horizontal sync pulses. These are then utilised to synchronise its own internal line and field oscillators.

Horizontal Oscillator

The horizontal oscillator with its peripheral components C66, R70 and RV9 on pin 15, and output at pin 11, can start operating at a low supply current, typically ≥4mA at pin 16, and is thus fed direct from the main HT rail. At 4mA the voltage at pin 16 is 5.5V and the line oscillator will start under these conditions. The duty factor of the horizontal output signal during this start up period is approximately 65%. At this stage pin 10 of IC4 is at zero potential since the line derived 12V supply is fed via a delay stage (TR12 and associated components) to ensure correct start up procedure for the IC.

The start of other IC4 functions is dependent on this main 12V supply at pin 10. As the supply volts rise, at the $5\cdot5V$ point all IC functions with the exception of the second phase detector (oscillator to flyback pulse) start working. The output voltage of the second phase detector at pin 14 is clamped internally, ensuring that the duty factor of the line drive at pin 11 stays at 65%.

As the voltage on pin 10 rises to 8.8V, the supply current for the line oscillator and output stage is now delivered via pin 10, freeing pin 16 of most of its load and allowing it to rise and stabilise at 8.7V. This change removes the clamping on pin 14 and this activates the second phase detector. From this point on, the

automatic correction for switch off delays (storage time) in the horizontal output stage is operative. Good stability is achieved by means of two feedback loops. In the first loop, the phase of the horizontal sync signal is compared with a waveform, of which the rising edge is referred to the top of the horizontal oscillator signal. In the second, the phase of the flyback pulse, which is derived from the collector of the line output transistor, is fed to pin 12 and compared with another reference waveform-the timing of which is such that the top of the flyback pulse is situated symmetrically on the horizontal blanking interval of the video signal.

The first phase detector is gated with a signal composed of the flyback pulse and a pulse derived from the horizontal output signal. This gating (slow time constant) is switched off during the acquisition of a signal. The output current of the phase detector is increased fivefold during this acquisition time and also under VCR conditions (fast time constant).

This means that the first loop has good noise immunity, whilst the second loop can be as fast as desired for compensation of switch off delays in the horizontal output stage.

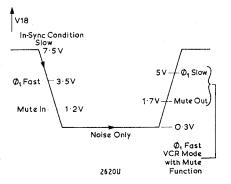
The first phase detector is inhibited during the retrace time of the vertical oscillator.

Horizontal picture shift is achieved by charging or discharging C65, connected to pin 14 of IC4.

Video and Sync Separator

Composite video is fed to pin 5 of IC4 via the low pass filter R63 and C63. The slicing level of the sync separator is set by R75 connected between pins 6 and 7. This level is independent of the amplitude of the sync pulse at the input of the IC. Nominal black level is 3·1V, the amplitude selective noise inverter becomes operative at 0·7V.

Vertical sync separation is accomplished with the aid of C78 on pin 4 of IC4.



The 'in-sync', 'out-of-sync', or 'no video' condition is detected by a valid signal identification/coincidence detector circuit at pin 18 of IC4. The voltage on pin 18 defines the time constant and gating of the first phase detector. To obtain correct operation of the IC for VCR and other AV functions, pin 18 is forced to a particular d.c. voltage by R69. If 12V is applied to the base of TR11 by selection of AV either at a channel selector button or by remote control, TR11 conducts and effectively earths R69. Thus under off-air reception conditions, the voltage at pin 18 is 6.9V. For AV operations the voltage is reduced to 3.0V.

Continued . . .

If the valid signal identification circuit senses that there is no valid signal available, it pulls pin 13 low, causing D23 to effectively mute the sound. The muting function is equally applicable when the incoming signal, or lack of it, is VCR derived.

Pin 13 of IC4 is a tri-state pin. One of the operating conditions being as described previously, that is with the pin at zero potential, sound muting is achieved. The other two states will be described later.

Vertical Oscillator

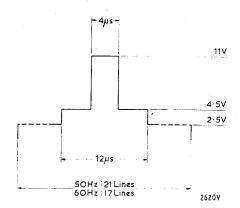
IC4 also contains a synchronised vertical oscillator and sawtooth generator. The oscillator signal is connected to the internal comparator, the other side of which is connected to pin 2 via an inverter and amplitude divider stage. The output of the comparator drives an emitter follower output stage internally connected to pin 1. To ensure a linear sawtooth at the oscillator, the load resistance at pin 3, R77 and the frame hold control RV10, is fed from the 26V supply and is connected directly to the charging capacitor C72. This ensures that the sawtooth amplitude is not affected by the supply at pin 10.

Feedback from the frame output stage is applied at pin 2 of IC4, and is compared with the sawtooth signal at pin 3. To optimise linearity and minimise picture bounce, the sawtooth signal is internally pre-corrected by 6% (convex), referred to pin 2. The linearity of the vertical deflection current depends on the oscillator signal at pin 3 and the feedback signal at pin 2.

A stabilised 6.5V reference source is provided within IC4 for the supply and reference of the vertical oscillator and comparator stage. This minimises interaction between horizontal and vertical components within the IC.

The output drive signal from pin 1 is also modified by the 50Hz/60Hz detector internally. This involves tri-state pin 13. Reception of a normal valid 50Hz signal leaves this pin at 12V whilst a valid 60Hz signal causes it to drop to 7.5V. The amplitude from pin 1 is thereby adjusted so that the picture height remains constant whilst in either mode.

IC4 also incorporates a vertical guard circuit, which monitors the vertical feedback signal at pin 2. If this level falls below 3·35V, or rises above 5·15V, the guard circuit inserts a continuous level of 2·5V into the sandcastle output signal at



pin 17. This will result in complete blanking of the screen. The sandcastle pulse generated at pin 17, has three different levels. The highest level 11V, is used for burst gating and black level clamping. The second level 4.6V, is obtained from the horizontal flyback pulse at pin 12 and is used for horizontal blanking. The third level 2.5V, is used for vertical blanking and is derived by counting the horizontal frequency pulses. For 50Hz the blanking pulse duration is 21 lines, for 60Hz it is 17 lines. The blanking pulse duration and sawtooth amplitude are automatically adjusted via the 50Hz/60Hz detector.

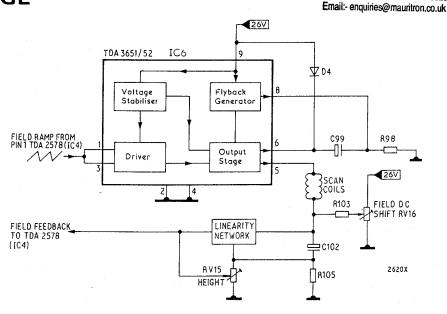
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FIELD OUTPUT STAGE

The field output stage comprises the field output IC6, a linearity/feedback network, d.c. shift and the appropriate feeds to the diode modulator stage in the 110° receiver. The field output IC6 is a TDA3651 for the 90° tube version and a TDA3652 for the 110° tube version. The ICs differ only in mechanical construction, and in the peak to peak current they can deliver to the scan coils. The drive signal from IC4 is connected to pin 1 and pin 3 which is also the input of a switching circuit. When flyback starts, this switching circuit rapidly turns off the lower output stage and so limits turn-off dissipation. It also allows the flyback generator to quick start.

In order to scan from a comparitively low supply rail, a flyback generator is incorporated in the IC. During scan, C99 at pin 6, is charged to a maximum voltage which is equal to the supply voltage of 26V applied to pin 9. When the flyback starts and the voltage at the output pin 5 exceeds that at pin 9, the flyback generator is activated. Then the supply voltage is connected in series, via pin 8, with voltage across C99. The voltage at the supply pin 6 of the output stage would then be twice the supply voltage. R98 on pin 8 adjusts this voltage so that the maximum rating of the IC is not exceeded.



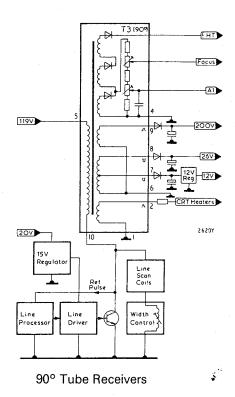
A thermal protection circuit is incorporated within the IC to protect against too high a dissipation. This circuit is active at 175°C which then reduces the deflection current in order to decrease dissipation.

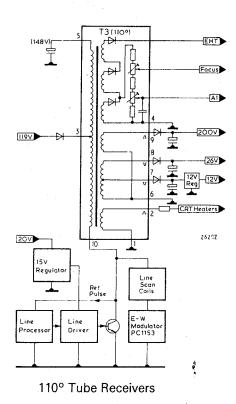
The output waveform from pin 5 is connected to the scan coils, then to the coupling capacitor, and finally to the feedback resistor R105. The height

potentiometer is connected across this resistor and feeds back, via R99, to the summing point of the linearity adjusting network R100, R101, R102, C101. R102 is fixed in 90° tube versions but is replaced by RV5 in 110°. The feedback is finally returned to the comparator at pin 2 of IC4.

Vertical picture shift is accomplished by bleeding in d.c. from RV16 and R103 to one side of the scan coils.

LINE OUTPUT STAGE





The line drive from IC4 is a.c. coupled to the line driver transistor TR8. IC9 provides a regulated 15V supply derived from the 20V rail of the switched mode power supply. The regulator has internal current limiting at 500mA and thermal shutdown protection, making the driver stage safe under fault conditions.

The driver transformer T2 provides all the necessary drive and base current shaping for the line output transistor TR10. R129 and C127 limit the peak collector voltage on the driver transistor TR8.

The diode split line output transformer T3 provides the line scan current and EHT. T3 also generates the following four supply lines from auxiliary windings:

Pin 9 provides the video output supply of 200V, rectified by D19 and smoothed by C130.

Pin 7 is the small signal 16V supply, rectified by D21 and smoothed by C135 and further processed by IC8 to produce 12V. IC8 contains current limiting and thermal overload protection. A take-off from pin 7 of the transformer, via R135, also provides a negative going line reference pulse for auxiliary control circuitry.

Pin 8 provides the frame output stage 26V supply, rectified by D25 and smoothed by C136.

Pin 2 is the CRT heater a.c. supply. Since not all CRTs have identical heater current requirements, the series resistor R622, which may be varied in value, is fitted on the CRT base PCB. The line output transformer T3, also rectifies two variable supplies internally for focus and A1 potentials. Two presets on the line output transformer assembly control these supplies, which are fed directly to the CRT base PCB.

The 90° tube version of the chassis has an HT supply of 119V. During flyback, both the line output transistor TR10, and the recovery diode D26, are off and the LOPT T3 is tuned by C134. Immediately after flyback, TR10 is turned on and both TR10 and D26 conduct. As the line scan current becomes positive, D26 turns off, leaving TR10 to complete the rest of the scan. C137 couples the line scan coils to provide 'S' correction.

The network C138, D24 and R138 maintains a constant charge on C137 during flyback at high beam currents. L18 provides linearity correction and is a preset coil which requires no adjustment. L19 is a variable inductor for width adjustment.

The line output stage of the 110° tube version of the chassis differs in that an HT supply of 148V is required. This is achieved by boosting the main HT rail to 148V within the line output transformer, C139 acting as smoothing capacitor. Adjustment is made by the SET HT potentiometer (RV13) for 148V, as measured on pin 5 of T3 at zero beam current.

Some other components change to support the higher scan currents required by 110° CRTs. Inspection of the main circuit diagram will show that it has been drawn for a 90° chassis, with annotations where 110° scanning necessitates changes.

Some CRTs used with the TX100 chassis require East-West raster correction. This is achieved in production by removing link 33 and fitting link 79 instead of L19 and R142 (width adjustment). The diode modulator board PC1153 is then fitted in order to provide the necessary correction.

DIODE MODULATOR BOARD, PC1153 (110° tube versions)

TR71 and TR72 on the diode modulator board PC1153, form a differential amplifier driving directly into the Darlington pair TR73. TR73 is the active element which provides width correction; it is adjusted by RV72.

To overcome the pincushion distortion factor of the CRT, more line width is required at the centre of the frame scan than at the top and bottom. The frame current parabola provides the necessary correction signal and this is fed to TR72 base via R712. TR71 is given an opposing signal via R708 from the pincushion correction potentiometer RV71. RV71 is

fed with both frame parabola and frame ramp waveforms, the wiper controlling the proportion of each waveform applied for correction.

The varying influence of TR73, effectively in series with the scan coils, would normally cause the EHT to vary. This is overcome by the use of a diode modulator. The flyback tuning, which controls the EHT, is determined by the series capacitance of C134 and C702. In the first limit case, when TR73 is fully off, the tuning capacitance will be approximately 6·8nF. In the second limit case, when TR73 is fully on, C702 will be short circuited by TR73 through L701 and

L702. Thus the tuning capacitance will be determined by C134 only, that is 10nF. Variations within these limits will provide EHT control. D26 and D701 discharge the two capacitors C134 and C702 after flyback, and also share the initial scan current with TR10. The tracking of this circuit with width variation provides a constant level of EHT. L701 stands off the reactance of C703, thus preventing it from affecting the tuning capacitance. C703 passes the major part of the scan current, whilst a proportion is fed to TR73, through L702, for width control.

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COMPONENT DETAILS & FUNCTIONS

♠ Denotes safety components.

Main Board (PC1150)

The PCB assembly is not available separately but is supplied as part of the TX100 basic chassis assembly.

90° tube version without remote control (PC1150-001)

90° tube version with remote control (PC1150-011)

110° tube version (PC1150-111)

*These components differ between 90° tube versions and 110° tube versions. The 110° tube versions are shown in brackets.

RESISTORS

- R1 47kΩ 5% 0-25W, R5470-GF02-01RG Sets the AFC range (with R3 and Z1)
- R2 1kΩ 5% 0·25W, R4100-GF02-01RG AFC defeat switch feed
- R3 2·2MΩ 5% 0·5W, R7220-GF05-04RG See R1
- R4 68kΩ 5% 0-25W, R5680-GF02-01RG AFC reference voltage divider (with R5)
- R5 68kΩ 5% 0·25W, R5680-GF02-01RG See R4
- R6 3·3kΩ 5% 0·25W, R4330-GF02-01RG RE AGC potential divider (with R10)
- R8 330kΩ 5% 0 · 25W, R6330-GF02-01RG AGC threshold level
- R10 1kΩ 5% 0·25W, R4100-GF02-01RG See R6
- R13 390Ω 5% 0·25W, R3390-GF02-01RG Impedance matching (with C19)
- R14 330Ω 5% 0·25W, R3330-GF02-01RG RF AGC feed
- R15 100Ω 5% 0+25W, R3100-GF02-01RG Video mute feed
- **R16** 680Ω 5% 0•25W, R3680-GF02-01RG AGC filter (with C22, C24)
- R17 2·2kΩ 5% 0·25W, R4220-GF02-01RG Part 6MHz trap (with L5, C56, C57)
- R18 1·5kΩ 5% 0·25W, R4150-GF02-01RG Video feed to sweep tune board
- R19 2-2kΩ 5% 0-25W, R4220-GF02-01RG Damping for 6MHz trap
- R20 100Ω 5% 0·25W, R3100-GF02-01RG TR1 base feed
 R21 470Ω 5% 0·25W, R3470-GF02-01RG
- TRT emitter load R22 910Ω 5% 0+25W, R3910-GF02-01RG
- P10Ω 5% 0-25W, R3910-GF02-01RG
 D. L. termination and trap isolation (with R23)
- **R23** 910Ω 5% 0+25W, R3910-GF02-01RG See R22
- R24 1.5kΩ 5% 0.25W, R4150-GF02-01RG Chroma feed pot down (with R26)
- R25 39kΩ 5% 0+25W, R5390-GF02-13RG AGC decoupling (with C18, IC2) R26 15kΩ.5% 0+25W, R5150-GF02-01RG
- R26 15kΩ 5% 0+25W, R5150-GF02-01RG See R24 R27 560Ω 5% 0+25W, R3560-GF02-01RG
- Luma feed pot down (with R28)

 R28 1-5kΩ 5% 0-25W, R4150-GF02-01RG
- 1-5kU 5% 0-25W, R4150-GF02-01RG See 827
- R29 39kΩ 5% 0-25W, R5390-GF02-01RG Part of colour control network (with R30, R31)
- **R30** 15kΩ 5% 0•25W, R5150-GF02-01RG See R29
- **R31** 68kΩ 5% 0·25W, R5680-GF02-01RG Sec R29

- R32 47kΩ 5% 0·25W, R5470-GF02-01RG Contrast control feed
- R33 18kΩ 5% 0·25W, R5180-GF02-01RG Contrast control pot divider (with R34)
- **R34** 68kΩ 5% 0 · 25W, R5680-GF02-01RG See R33
- R35 10Ω 5% 0-25W, R2100-GXP2-W097 HT fusible resistor
 - R36 18kΩ 5% 0-25W, R5180-GF02-01RG Brightness control feed
 - R37 8·2kΩ 5% 0·25W, R4820-GF02-01RG Brightness control pot divider (with R38)
 - R38 100kΩ 5% 0-25W, R6100-GF02-01RG See R37
 - R39 390Ω 5% 0-25W, R3390-GF02-01RG Chroma delay line feed
 - R40 470Ω 5% 0-25W, R3470-GF02-01RG Pot divider for D°L balance adjustment (with RV4)
 - R41 470Ω 5% 0-25W, R3470-GF02-01RG DL 1 impedance matching
 - R42 100Ω 5% 0·25W, R3100-GF02-01RG TR2 emitter load
 - R43 100Ω 5% 0·25W, R3100-GF02-01RG TR61 base feed
 - R44 620 Ω 5% 0-25W, R3620-GF02-01RG Beam current sensing resistor
 - R46 100Ω 5% 0·25W, R3100-GF02-01RG TR63 base feed
 - R48 180kΩ 5% 0·25W, R6180-GF02-01RG Line reference pulse current limiting
 - R49 4-7kΩ 5% 0-25W, R4470-GF02-01RG AFC line decoupling (with C17)
 - **R50** 15kΩ 5% 0·25W, R5150-GF02-01RG Start-up delay bias (with R51)
 - R51 15kΩ 5% 0·25W, R5150-GF02-01RG See R50
 - **R52** 820Ω 5% 0+25W, R3820-GF02-01RG D.C. feed to pin 7 of IC2
 - R54 33kΩ 5% 0·25W, R5330-GF02-01RG Phase detector d.c. load
 - R55 1kΩ 5% 0+25W, R4100-GF02-01RG Phase detector damping
 - R56 33kΩ 5% 0·25W, R5330-GF02-01RG Phase detector d.c. load
 - **R57** 220Ω 5% 0-25W, R3220-GF02-01RG Data blanking pull-down
 - R58 15kΩ 5% 0-25W, R5150-GF02-01RG Part of 12V delay circuit to IC4 (with C62)
- R59 1kΩ 5% 0·25W, R4100-GF02-01RG Sandcastle pulse feed
- R60 82kΩ 5% 0·25W, R5820-GF02-01RG
 Automatic cut-off bias (with R61)
 R61 130kΩ 5% 0·25W, R6130-GF02-01RG
- See R60 R62 100Ω 5% 0·25W, R3100-GF02-01RG
- TR65 base feed

 R63 1.5kΩ 5% 0.25W, R4150-GF02-01RG
- Part video low-pass filter (with C63) **R64** 47kΩ 5% 0-25W, R5470-GF02-01RG
- Part d.c. divider network for line shift R65 6·8kΩ 5% 0·25W, R4680-GF02-01RG
- Part TR11 base bias (with R67)
 R66 47Ω 5% 0-25W, R2470-GF02-01RG
- 24V HT feed dropper R67 1·8kΩ 5% 0·25W, R4180-GF02-01RG
- See R65

 R68 82·5kΩ 1% 0·25W, R5825-BM02-08RG
- **R68** 82 · 5kΩ 1% 0 · 25W, R5825-BM02-08R0 Line shift d.c. feed
- R69 270kΩ 5% 0+25W, R6270-GF02-01RG Coincidence detector level set
- R70 36+5kΩ 1% 0+25W, R5365-BM02-08RG Part line oscillator network (with C66, RV9)
- R71 15kΩ 5% 0-25W, R5150-GF02-01RG Valid signal detector pull-up resistor
- R72 82Ω 5% 0-25W, R2820-GF02-01RG Sync separator time constant (with C70)
- R73 9-1kΩ 5% 0-25W, R4910-GF02-01RG Horizontal output, IC4 pin 11 load
- R74 100Ω 5% 0-25W, R3100-GF02-01RG Horizontal output drive buffer
- **R75** 5+6kΩ 5% 0+25W, R4560-GF02-01RG Sync slicing level set (with C71)
- R76 220Ω 5% 0-25W, R3220-GF02-01RG
 Sandcastle pulse output buffer
 R77 180kΩ 5% 0-25W, R6180-GF02-01RG
- Part field oscillator (with RV10, C72)

 R78 18kΩ 5% 2W, R5180-GX02-30RG

 HT series dropper for IC4

- *R79 27kΩ 5% 0-5W, R5270-GC05-10RG (24kΩ 5% 0-5W, R5240-GC05-10RG)
 Line fly-back pulse pot divider (with R139, R140,
- R80 470Ω 5% 0-25W, R3470-GF02-01RG
 Part phase detector time constant (with C77)
- R82 82kΩ 5% 0-25W, R5820-GF02-01RG
 Damping of sound quadrature coil
- R83 470Ω 5% 0-25W, R3470-GF02-01RG Sound IF input impedance matching
- **R84** 470Ω 5% 0·25W, R3470-GF02-01RG IC5 input matching
- **R85** 4-7k Ω 5% 0-25W, R4470-GF02-01RG Part load and de-emphasis for low level audio (with C80)
- R86 1kΩ 5% 0·25W, R4100-GF02-01RG Minimum volume tracking
- R87 1kΩ 5% 0-25W, R4100-GF02-01RG Part of treble control network (with C86, C87, C88
- R88 150Ω 5% 0·25W, R3150-GF02-01RG Audio frequency response network (with C91)
- **R89** 39kΩ 5% 0-25W, R5390-GF02-01RG Audio gain setting (with R90)
- R90 5.6kΩ 5% 0.25W, R4560-GF02-01RG See R89
- **R91** 4·7Ω 5% 0·5W, R1470-GXP5-W090 Audio output damping (with C93)
 - **R92** 15kΩ 5% 0·25W, R5150-GF02-01RG 12V supply limiting to IC5 pin 6
 - R93 470Ω 5% 0+25W, R3470-GF02-01RG External volume/mute option
 - R94 1-2Ω 5% 0-25W, R1120-GM02-07RG
 Part field output damping network (with R104, C103)
- ↑ R95 2 · 2Ω 5% 0 · 25W, R1220-GXP2-W102 Supply smoothing
 - **R96** 6·8kΩ 5% 0·25W, R4680-GF02-01RG Field ramp drive network (with C95)
- 4·7Ω 5% 0·25W, R1470-GM02-19RG (0·68Ω 5% 0·25W, R0680-GM02-RS29) 26V feed resistor to IC6
- *R98 820Ω 5% 0·25W, R3820-GF02-17RG (560£ 5% 0·25W, R3560-GF02-01RG)
- Field fly-back boost resistor

 *R99 27kΩ 5% 0·25W, R5270-GF02-01RG
- (18kΩ 5% 0+25W, R5180-GF02-01RG)
 Part field linearity network (with R100, R101, R102)
 *R100 47kΩ 5% 0+25W, R5470-GF02-01RG
- (27kΩ 5% 0·25W, R5270-GF02-01RG) See R99
- *R101 8·2kΩ 5% 0·25W, R4820-GF02-01RG (6·8kΩ 5% 0·25W, R4680-GF02-01RG) See R99
- *R102 510Ω 5% 0·25W, R3510-GF02-01RG (RV5) See R99
- *R103 470Ω 5% 0·5W, R3470-GF05-04RG (220Ω 5% 0·5W, R3220-GF05-04RG) D.C. feed for field shift
- R104 390Ω 5% 0+25W, R3390-GF02-01RG See R94
- *R105 1·5Ω 5% 0·5W, R1150-GXP5-W090 (0·68Ω 5% 0·5W, R0680-GXP5-W090) Field output current feedback resistor
- R106 1-8Ω 10% 3W, R1180-SW03-W093
 Mains surge current limiting
- R107 1MΩ 20% 0.5W, R7100-WC05-10RG Part of RFI suppression network (with C109, L13)
- R108 220Ω 5% 0·25W, R3220-GF02-01RG Start-up timing component (with C112)
- R109 1-2kΩ 5% 0-25W, R4120-GF02-01RG
 Part of SET HT por divider (with R110, RV13)
- R110 12kΩ 5% 0-25W, R5120-GF02-01RG See R109
- R111 100kΩ 5% 0+25W, R6100-GF02-01RG
 Holds standby pin in ON condition
 R112 10kΩ 5% 0+25W, R5100-GF02-01RG
- Gives 'zero crossing' information to IC7
- R113 100Ω 5% 2W, R3100-GX02-30RG Part delay on 'zero crossing' (with C115)
- R114 0-68Ω 5% 0-25W, R0680-GM02-RS29
 Ensures correct TR6 base drive
- R115 300kΩ 5% 0+5W, R6300-GM05-MU21
 Provides facsimile of collector current to IC7 (with C118)
- R116 4·7kΩ 5% 4W, R4470-GW04-22RG
 Supplies initial start-up current
 R117 100kΩ 5% 0·25W, R6100-GF02-01RG
- Provides SCR1 gate current (with R118)
 R118 100kΩ 5% 0+25W, R6100-GF02-01RG
 See R117

- R119 560Ω 5% 0·25W, R3560-GF02-01RG Zener stand-off resistor, after start-up
- R120 1k Ω 5% 0·25W, R4100-GF02-01RG Pre-load for 9V supply during standby
- R121 27Ω 5% 0-25W, R2270-GF02-01RG
 Part of TR6 base drive network
- R122 6·8kΩ 5% 4W, R4680-GW04-21RG Pre-load for HT rail during standby
- Λ* R123 10MΩ 5% 0·5W, R8100-GF05-RS31 (3·3MΩ 5% 0·5W, R7330-GF05-RS31) Chassis leakage (with C122)
 - R124 10kΩ 5% 0·25W, R5100-GF02-01RG TR7 base bias (with R125)
 - R125 100Ω 5% 0·25W, R3100-GF02-01RG See R124
 - *R126 Replaced by LK77
 (47Ω 5% 0-25W, R2470-GF02-01RG)
 Part of height network
 - R127 8·2kΩ 5% 0·25W, R4820-GF02-01RG TR8 base load
 - R128 27k Ω 5% 0 · 25W, R5270-GF02-01RG TR9 base bias
 - R129 120Ω 5% 0·25W, R3120-GF02-01RG Part of T2 tuning (with C127) R130 150Ω 5% 1W. R3150-GF10-E193
 - R130 150Ω 5% 1W, R3150-GF10-E193 Set relay current
 - R131 6·8Ω 5% 0·5W, R1680-GF05-04RG Part of T3 tuning (with C133, L17) R132 47Ω 5% 0·25W, R2470-GF02-01RG
 - TR10 base load
 - R133 0·22Ω 5% 0·25W, R0220-GM02-RS29 26V rail surge limiting R134 1·2kΩ 5% 7W, R4120-GW07-VM84
 - Discharges C120 during TR6 ON period R135 56kΩ 5% 0 · 25W . R5560-GF02-01RG
 - R135 56kΩ 5% 0·25W, R5560-GF02-01RG Fly-back pulse pot divider (with R137) R136 1kΩ 5% 1·5W, R4100-GX01-W107
 - L18 'Q' limiting R137 39kΩ 5% 0·25W, R5390-GF02-01RG
- See R135
 *R138 3-3kΩ 5% 0-5W, R4330-GF05-04RG
 (Deleted)
 Part of 'S' correction damping network (with C137 C138, D24)
- *R139 Replaced by LK85 (24kΩ 5% 0·5W, R5240-GC05-10RG) See R79
- R140 100kΩ 5% 1W, R6100-GM10-MU20 See R79
- *R141 6·8kΩ 5% 0·25W, R4680-GF02-17RG (5·6kΩ 5% 0·25W, R4560-GF02-01RG) See R79
- *R142 1kΩ 5% 1·5W, R4100-GX01-W107 (LK79)
 L19 'Q' limiting
- * R143 27Ω 5% 0·25W, R2270-GF02-17RG (15Ω 5% 0·5W, R2150-GXP5-W090) Driver current limiting
- **Z1** VDR P15 2/1R, 00E5-146-PD1 See R1
- Z2 Dual PTC Thermistor, 00E5-147-MU1 Degauss PTC

VARIABLE RESISTORS

- RV4 1kΩ Lin. 10mm preset pot., 00E1-131-410-PH1 Chroma D/L balance adjustment
- *RV5 Replaced by R102 in 90° chassis (4.7kΩ Lin. 10mm preset pot., 00E1-131-447-PH1) Field linearity adjustment
- RV8 $47k\Omega$ Lin. 10mm preset pot., 00E1-131-547-PH1 Line phase adjustment
- RV9 $10k\Omega$ Lin. 10mm preset pot., 00E1-137-510-PH4 Line hold adjustment
- $\mbox{RV10}$ 220k Ω Lin. 10mm preset pot., 00E1-131-622-PH1 Field hold adjustment
- RV13 4.7k Ω Lin. 10mm preset pot., 00E1-131-447-PH1 Set HT adjustment
- RV15 100Ω Lin. 10mm preset pot., 00E1-131-310-PH1 Height adjustment
- RV16 1kΩ W/W hor. preset pot., 90E1-014-410-EG1 Field shift adjustment

CAPACITORS

- C1 100nF +80% -20% 16V, C6100-EW216-MAK6 AFC decoupling C3 10nF +80% -20% 50V, C5100-EW250-MAK3
- C3 10nF +80% -20% 50V, C5100-EW250-MAK3 AFC defeat line coupling
- C5 10nF +80% -20% 50V, C5100-EW250-MAK3 Tuning voltage decoupling
- C6 22μF 20% 50V Elec., CE222-MS250-10CG Tuner AGC voltage decoupling

- C7 220nF 10% 100V, C6220-SS310-04CG Tuning voltage decoupling
- C9 100μF 20% 16V Elec., CE310-MS216-10CG 12V rail decoupling
- C10 68pF 5% 50V, C2680-GG250-TY16 Bottom end coupling
- C11 150pF 5% 50V, C3150-GG250-MAK5 Part preamp input circuit (with C12, L1)
- C12 18pF 5% 50V, C2180-GG250-MAP4 See C11
- C13 15pF 5% 50V, C2150-GG250-MAJ4 Video shaping
- C15 10nF +80% -20% 50V, C5100-EW250-MAK3 IC1 12V supply decoupling
- C16 1μF 20% 50V Elec., CE110-MS250-10CG IC1 AGC decoupling
- C17 100nF +80% -20% 16V, C6100-EW216-MAK6 See R49
- C18 1μF 20% 50V Elec., CE110-MS250-10CG See R25
- C19 10nF 30% 25V, C5100-TT225-TY14 See R13
- C20 100nF 10% 63V, C6100-SS263-17CG IC2 12V supply RF decoupling
- C21 10nF 30% 25V, C5100-TT225-TY14 D.C. feedback loop decoupling
- C22 1μF 20% 50V Elec., CE110-MS250-10CG See R16
- C23 56pF 5% 50V, C2560-GG250-SI26 L2 tuning
- C24 10nF +80% -20% 50V, C5100-EW250-MAK3 See R16
- C25 82pF 5% 50V, C2820-GG250-Si26 L3 tuning
- C26 56pF 5% 50V, C2560-GG250-MAJ7
- Makes the noise in the AFC circuit symmetrical
 C27 10pF 5% 50V, C2100-GG250-TY15
 Part of 4·43MHz filter (with L6)
- C28 1μF 20% 50V Elec., CE110-MS250-10CG Luma input feed
- C29 10nF 30% 25V, C5100-TT225-TY14 Chroma input feed
- C30 120pF 5% 50V, C3120-GG250-MAK5 Chroma filter tuning (with L7)
- C31 100nF 10% 63V, C6100-SS263-17CG Colour control decoupling
- C32 47µF 20% 16V Elec., CE247-MS216-10CG Contrast control decoupling
- C33 33µF 20% 25V Elec., CE233-MS225-10CG HT decoupling
- C34 100nF 10% 63V, C6100-SS263-17CG HT decoupling
- C35 22µF 20% 50V Elec., CE222-MS250-10CG Brightness control decoupling
- C36 10nF +80% -20% 50V, C5100-EW250-MAK3 Chroma D/L coupling
- C37 10nF +80% -20% 50V, C5100-EW250-MAK3 Chroma D/L matrix drive
- C39 470nF 20% 50V Elec., CE047-MS250-10CG Beam limiter loop damping
- C40 27pF 5% 50V, C2270-GG250-TY15 Luminance compensation
- C43 4-7µF 20% 50V Elec., CE147-MS250-10CG ACC time-constant
- C44 330nF 10% 63V, C6330-SS263-17CG Ident time-constant
- C45 470nF 10% 63V, C6470-SS263-17CG Green black level storage
- C46 100nF 10% 63V, C6100-SS263-17CG Phase detector HF filter
- C47 2·2µF 20% 25V Elec., CE122-MS225-14CG Phase detector LF filter
- C48 100nF 10% 63V, C6100-SS263-17CG Phase detector HF filter
- C50 470nF 10% 63V, C6470-SS263-17CG Blue black level storage
- C51 470nF 10% 63V, C6470-SS263-17CG Red black level storage
- C52 1µF 20% 50V Elec., CE110-MS250-11CG Leakage current storage
- C53 100pF 5% 50V, C3100-GG250-MAJ7 Twice subcarrier trap
- C54 47μF 20% 25V Elec., CE247-MS225-10CG Start-up delay
- C56 330pF 5% 630V, C3330-GG363-RBF9 See R17
- C57 330pF 5% 630V, C3330-GG363-RBF9 See R17
- C62 22μF 20% 50V Elec., CE222-MS250-10CG See R58
- C63 150pF 10% 50V, C3150-SS250-TY12 See R63

- C64 100nF 10% 63V, C6100-SS263-17CG Coincidence detector filter
- C65 47nF 10% 250V, C5470-SS325-04CG Second phase detector filtering
- C66 2-2nF 1% 160V, C4220-BB316-RBF9 See R70
- C67 100nF 10% 63V, C6100-SS263-17CG 12V supply decoupling
- 12V supply decouplingC68 220μF 20% 16V Elec., CE322-MS216-20CG12V supply decoupling
- C69 10μF 20% 50V Elec., CE210-MS250-10CG Valid signal detector decoupling
- C70 22μF 20% 50V Elec., CE222-MS250-10CG See R72
- C71 1µF 20% 50V Elec., CE110-MS250-10CG See R75 C72 470nF 10% 63V. C6470-SS263-05CG
- See R77
 C73 100nF 10% 63V, C6100-SS263-05CG
- C73 100nF 10% 63V, C6100-SS263-17C0 HT supply decoupling C74 1nF 10% 50V, C4100-SS250-TY12
- Flyback pulse coupling
- C75 1μ F 20% 50V Elec., CE110-MS250-10CG HT supply decoupling
- C76 330nF 10% 63V, C6330-SS263-17CG IC4 pin 8 decoupling
- C77 10μF 20% 50V Elec., CE210-MS250-10CG
- See H80

 10μF 20% 50V Elec., CE210-MS250-10CG
 Field sync integrating capacitor
- C79 33pF 5% 50V, C2330-GG250-TY15
- Decoupling capacitor, sound take-off C80 10nF 30% 25V, C5100-TT225-TY14
- See R85

 C81 22nF 30% 16V, C5220-TT216-TY25

 IF decoupling
- C82 5-6pF 10% 50V, C1560-SS250-TY15
 Part of sound detector coil tuning
- C83 47μF 20% 16V Elec., CE247-MS216-10CG Ripple decoupling
- C84 1µF 20% 50V Elec., CE110-MS250-10CG Volume control decoupling C86 6·8nF 20% 25V, C4680-WW225-TY14
- See R87
 C87 2-2nF 20% 50V, C4220-WW250-TY19
- See R87
 C88 22nF 30% 16V, C5220-TT216-TY25
- See R87
 C89 220nF 10% 63V, C6220-SS263-17CG
- 20V supply decoupling, IC5 pin 10
 C90 1000µF 20% 35V Elec., CE410-MS235-21CG
 20V supply smoothing
- 20V supply smoothing
 C91 47μF 20% 16V Elec., CE247-MS216-10CG
 See R88
- C92 22nF 30% 16V, C5220-TT216-TY25 Bass boost capacitor
- C93 68nF 10% 63V, C5680-SS263-17CG See R91
- C94 470μF 20% 50V Elec., CE347-MS250-21CG D.C. blocking, LS coupling
- C95 10nF +80% -20% 50V, C5100-EW250-MAK3
- C96 390pF 10% 50V, C3390-SS250-TY12 Parasitic quencher
- C97 100nF 10% 63V, C6100-SS263-17CG 26V supply rail decoupling
- C98 220µF 20% 35V Elec., CE322-MS235-01CG 26V supply rail smoothing
- C99 100µF 20% 25V Elec., CE310-MS225-10CG Field flyback boost capacitor
- C100 2·7nF 10% 50V, C4270-SS250-MAG1 HF decoupling
- *C101 10μF 20% 50V Elec., CE210-MS250-23CG (3·3μF 20% 50V Elec., CE133-MS250-23CG) Part of field linearity network
- C102 1000µF 20% 25V Elec., CE410-MS225-01CG Field output coupling capacitor
- *C103 100nF 10% 100V, C6100-SS310-MUJ4 (330nF 10% 63V, C6330-SS263-17CG)
- C104 470pF 10% 2kV, C3470-SS420-MAM1
 Part diode bridge transient protection network (with
- C105, C106, C107)

 C105 470pF 10% 2kV, C3470-SS420-MAM1
 See C104
- C106 470pF 10% 2kV, C3470-SS420-MAM1 See C104 C107 470pF 10% 2kV, C3470-SS420-MAM1
- See C104 ^C108 100nF 20% 250V a.c., C6100-WW325-RBF4
- Mains filter

 100nF 20% 275V a.c., C6100-WW327-RF13
 See R107

C110 150µF +50% --10% 385V Elec., CE315-MS338-SM21 334V unstabilised rail reservoir

C111 100nF 10% 400V, C6100-SS340-04CG 334V rail decoupling

C112 22µF 20% 50V Elec., CE222-MS250-10CG See R108

C113 1µF 20% 50V Elec., CE110-MS250-10CG Facsimile reservoir capacitor C114 100pF 5% 50V, C3100-GG250-MAJ7

Frequency stabilizing for overload and no-load C115 8-2nF 5% 160V, C4820-GG316-LC61

See R113 C117 100µF 20% 16V Elec., CE310-MS216-10CG

Ensures correct base drive to TR6 C118 8·2nF 5% 160V, C4820-GG316-LC61

See R115 C119 22µF 20% 50V Elec., CE222-MS250-10CG

D12 reservoir C120 1·8nF 10% 1·5kV, C4180-SS415-RF12 Prevents over-dissipation in TR6 by reducing the rise-time of the collector volts.

C121 4·7µF 20% 160V Elec., CE147-MS316-RYH4 119V supply reservoir

C122 4700pF 20% 250V AC, C4470-WW325-RF14 See 8123

C123 470µF 20% 35V Elec., CE347-MS235-21CG

20V supply rail reservoir C124 220μF 20% 25V Elec., CE322-MS225-20CG 9V supply reservoir

C125 100nF 10% 63V, C6100-SS263-17CG TR8 base coupling

C126 330nF 10% 63V, C6330-SS263-17CG IC9 input decoupling

C127 10nF +80% -20% 50V, C5100-EW250-MAK3 See R129

C128 2.2µF 10% 160V, C7220-SS316-02CG

119V rail decoupling C129 100µF 20% 160V Elec., CE310-MS316-01CG 119V rail smoothing 100nF 10% 63V, C6100-SS263-17CG

IC8 output decoupling

C132 100nF 10% 63V, C6100-SS263-17CG IC8 input decoupling

C133 22nF 10% 250V, C5220-SS325-MUF6 See R131

*C134 7·5nF 5% 1500V, C4750-GG415-MUH8 (10nF 5% 2kV, C5100-GG420-MUH9)

Line flyback tuning C135 4·7μF 40V Elec., CE147-MV240-RBB5 16V smoothing

C136 2200µF 40V Elec., CE422-MS240-01CG 26V smoothing

*C137 470nF 10% 250V, C6470-SS325-RBG6 (330nF 5% 400V, C6330-GG340-10CG)

'S' corrector — see R138 *C138 1μF 20% 160V Elec., CE110-MS316-NNC1 (Deleted) See R138

*C139 (100µF 200V Elec., CE310-MS320-RYH1) T3 pin 5 smoothing

C140 12pF 10% 2kV, C2120-SS420-MAM1 Optimises line shift

C141 10µF 20% 50V Elec., CE210-MS250-10CG 15V rail decoupling

C143 4.7µF 20% 50V Elec., CE147-MS250-10CG Phase feed-back

CV49 2-22pF trimmer, 00E4-114-MU1 Crystal frequency adjustment

TRANSISTORS

Par

BC237B, 00TR-001-203-1TG Video emitter follower

BC237B, 00TR-001-203-1TG

TR3 BC237B, 00TR-001-203-1TG Start-up delay

TR6 T9063V, 01V0-958 Chooper transistor

ZTX650/STZA, 00V1-638 TR7 Switches off teletext during standby

BC372, 09V1-343 Line driver

TR9 BC237B, 00TR-001-203-1TG Switches off relay during standby

*TR10 T6071V, 01V0-973 (T6073V, 01V0-978) Line output transistor
TR11 BC237B, 00TR-001-203-1TG

AV inverter

TR12 BC307C, 00TR-004-204-1TG Part of 12V delay circuit

SCR1 T1CP 106D, 01V0-975 IC7 start-up switching

DIODES

D1 Type 425, 00DD-001-001-1DG Automatic cut-off isolation BZX79C/83C, 00DZ-0020-2105-1DG

D2 Beam limiter feed

D3 Type 425, 00DD-001-001-1DG Start-up delay catching

IN4002, 00DP-002-001-1DG Field flyback boost diode

D5 BY133GP, 03V4-117-200

Part of mains bridge rectifier (with D6-D8) D6 BY133GP, 03V4-117-200

See D5 BY133GP, 03V4-117-200 D7

See D5

BY133GP, 03V4-117-200 **D8** See D5

RGP5020, 02V4-725-200 D9

Facsimile rectifier Type 425, 00DD-001-001-1DG D10

SCR1 gate supply; switches off during normal-working D11 BZX79C83C, 00DZ-0020-1565-1DG

Set minimum gate voltage

RGP5020, 02V4-725-200 D12 IC7 supply rectifier IN4001, 00DP-001-001-1DG D13

Improves shape of TR6 base drive pulse

RGP10M, 01V4-786-200 D14 Quick charge-up of C120 when TR6 is off

BY299, 03V4-143-200 D15 119V supply rectifier

D16 IN5401, 02V4-517-200 9V supply rectifier

D17 Type 425, 00DD-001-001-1DG

Sets standby threshold (with D18) Type 425, 00DD-001-001-1DG D18 See D17

D19 RGP5100, 02V4-712-200

200V supply rectifier IN4001, 00DP-001-001-1DG Back EMF protection

RGP10G, 01V4-783-200 D21 16V supply rectifier

D22 RGP30B, 02V4-736-200

20V supply rectifier Type 425, 00DD-001-001-1DG D23

Audio muting diode RGP5040, 02V4-737-200 * D24 (Deleted) See R138

BYV95B, 03V4-148-200 D25 26V supply rectifier

*D26 BY127G, 03V4-123-200 (BY228, 00DP-010-001-1DG)

Efficiency diode (BY299, 03V4-143-200) * D28 Isolates oin 3 of T3 from 119V rail

Type 425, 00DD-001-001-1DG Beam limiter feed to brightness control (Type 425, 00DD-001-001-1DG)

(D31 replaces LK86) Reference diode

INTEGRATED CIRCUITS

SL1432, 00V3-610 SAW Filter preamp and RF AGC

IC2 TDA3540, 00V3-672

Vision IF amplifier and demodulator TDA3562A, 00V3-673 IC3

Luma-chroma processor and data input TDA2578A, 00V3-739

Sync and line processor TDA1701, 00V3-674 IC5

Sound IF and output *106 TDA3651, 00V3-679

(TDA3652, 00V3-644) Field output TDA4600-2, 00V3-571

Chopper control

MC7812CT, 00IC-011-901-1IG 12V regulator

MC78M15CT, 00V3-737 15V regulator

SW153A/F1045A, 00IC-009-301-1IG SAW Filter

INDUCTORS

Band pass coil, 06D0-254-002-TK1 Part band-pass pair with tuner output coil Carrier tank coil, 06D0-255-002-TK1

Vision reference carrier AFC coil, 06D0-256-002-TK1

AFC demodulator L4 3-3µH 20% Axial lead, L1330-WA000-01LG

Vision harmonic suppressor 5·5/6·0MHz Filter, 06D0-257-002-TK1

Part bridge tee filter L6 4-4MHz rejector, 00D0-913-002-TK1

4·43MHz filter

Pre-chroma delay line coil, 00D0-919-002-TK1 Chroma input filter Pre-chroma delay line coil, 00D0-919-002-TK1 L9

Phase adjustment L10 Post-chroma delay line coil, 00D0-920-002-TK1

Balance adjustment 1.12 6MHz Quadrature coil, 06D0-214-002-TK1

Sound detector coil L13 RFI Choke spec. T1011L, 00D4-241-001-DN1 RF interference suppression

6-8µH 10% Axial lead, L1680-SA000-01LG Anti-radiation choke

2.2µH 20% Axial lead, L1220-WA000-01LG TR6 base drive inductor

÷

6.8µH 1A 20% Axial, L1680-WA000-TD3 Anti-radiation choke

1 17 Harmonic tuning choke, 06D0-261-001-TK1 See R131

Linearity coil, 06D4-026-001 *L18 (Linearity coil, 06D4-028-001)

Linearity adjustment Width coil, 06D4-024-001 *L19

(Deleted) Width adjustment

6.8µH 1A 20% Axial, L1680-WA000-TD3 L21

Anti-radiation choke 123 Filter choke, 06D4-031-001 RFI suppressor

T1 PSU ISO Switched mode transformer, 06D3-082-001 Pulse transformer

T2 Line driver transformer, 06D4-023-001 Line drive

* T3 Diode split LOPT, 06D3-083-001 (Diode split LOPT, 06D3-087-001) Line output and EHT transformer

MISCELLANEOUS

CF1 6.0MHz ceramic filter, 00E5-992-MA3 Provides rejection of unwanted frequencies

DL1 Chroma delay line, 00E5-931-001-01G Chroma delay line Luminance delay line, 00E5-966-TD1

Luminance delay line

FB1 Ferrite bead assembly, 06D4-030-001 Anti-radiation choke

FS1 Fuse T1-6A time lag, 00E6-041-160-WN1 Mains input fuse

XL1 Crystal 8 · 8MHz, 00E5-941-001-01G Reference oscillator, runs at twice subcarrier frequency

OMI TS112M, 00D6-013-001 Switches HT off during standby

CRT Base Board

90° tube version (PC1174)

110° 30AX tube version (PC1173) Although the two versions of the PCB have physical differences, the components are identical and have the same circuit reference.

RESISTORS

R601 100kΩ 5% 0·5W, R6100-GF05-04RG

Green feedback R602 2·2kΩ 5% 0·25W, R4220-GF02-01RG Green bias

R603 15kΩ 5% 2W, R5150-GX02-30RG Green load

↑ R604 1kΩ 5% 0 · 25W, R4100-GXP2-WO97 Green beam current sampling feed R605 100kΩ 5% 0.5W, R6100-GF05-04RG Blue feedback

Continued . . .

R606 2·2kΩ 5% 0·25W, R4220-GF02-01RG

R607 15kΩ 5% 2W, R5150-GX02-30RG Blue load

↑ R608 1kΩ 5% 0 · 25W, R4100-GXP2-WO97 Blue beam current sampling feed

R609 100kΩ 5% 0.5W, R6100-GF05-04RG Red feedback

R610 2·2kΩ 5% 0·25W, R4220-GF02-01RG Red bias

R611 15kΩ 5% 2W, R5150-GX02-30RG Red load

↑ R612 1kΩ 5% 0·25W, R4100-GXP2-WO97 Red beam current sampling feed

R613 4·7kΩ 5% 0·25W, R4470-GF02-14RG

Video output reference voltage setting (with R618) **R614** 47Ω 5% 0 · 25W, R2470-GF02-RS28

Base feed, green ↑ R615 47Ω 5% 0 - 25W, R2470-GF02-RS28

Base feed, blue
Λ R616 47Ω 5% 0-25W, R2470-GF02-RS28 Base feed, red

R617 1kΩ 5% 0-25W, R4100-GF02-14RG Video output reference feed

R618 820Ω 5% 0·25W, R3820-GF02-01RG See R613

R619 100kΩ 5% 1W, R6100-GM10-MU20 A1 stand-off

R620 10kΩ 10% 0.5W, R5100-SC05-10RG Grid pot-down (with R623)

R621 2·7kΩ 10% 0·5W, R4270-SC05-10RG Blue stand-off

R622 3·3Ω 10% 1·5W fusible, R1330-SX01-W104 Heater dropper

15kΩ 10% 0·5W, R5150-SC05-10RG See R620

R624 2-7kΩ 10% 0-5W, R4270-SC05-10RG Green stand-off

R625 2·7kΩ 10% 0·5W, R4270-SC05-10RG Red stand-off

VARIABLE RESISTORS

RV61 10kΩ lin. 10mm hor. pot., 00E1-131-510-PH2 Green gain adjustment

RV62 $10k\Omega$ lin. 10mm hor. pot., 00E1-131-510-PH2 Blue gain adjustment

RV63 $10k\Omega$ lin. 10mm hor. pot., 00E1-131-510-PH2 Red gain adjustment

CAPACITORS

C601 39pF 5% 50V, C2390-GG250-TY15 Green compensation C602 39pF 5% 50V, C2390-GG250-TY15

Blue compensation

C603 39pF 5% 50V, C2390-GG250-TY15 Red compensation

C604 1µF 20% 50V Elec., CE110-MS250-23CG Video output reference decoupling

C605 4-7µF 20% 250V Elec., CE147-MS325-01CG HT decoupling

C606 10pF 5% 500V, C2100-GG350-MAR4 Decoupling

C607 10pF 5% 500V, C2100-GG350-MAR4 Decoupling

C608 10pF 5% 500V, C2100-GG350-MAR4 Decoupling

1nF 20% 50V, C4100-WW250-TY13 C609 Green compensation
C610 1nF 20% 50V, C4100-WW250-TY13

Blue compensation

1nF 20% 50V, C4100-WW250-TY13 Red compensation

C612 100nF 10% 250V, C6100-SS325-15CG

Grid decoupling 10nF +80% -20% 2kV, C5100-EW420-MAK8 A1 decoupling

C614 220µF 20% 15V Elec., CE322-MS216-26CG LT decoupling

TRANSISTORS

TR60 BC308C, 00TR-005-404-1TG Video output bias TR61 BF787, 00TR-033-801-1TG

Green amplifier

TR62 BF493S, 09V1-367

Green beam current sensing

TR63 BF787, 00TR-033-801-1TG Blue amplifier

TR64 BF493S, 09V1-367

Blue beam current sensing TR65 BF787: 00TR-033-801-1TG

Red amplifier

TR66 BF493S, 09V1-367

Red beam current sensing TR67 BF392, 00TR-027-401-1TG

Green emitter follower

TR68 BF392, 00TR-027-401-1TG Blue emitter follower

TR69 BF392, 00TR-027-401-1TG Red emitter follower

DIODES

D601 Type 425, 00DD-001-001-1DG

Green cathode feed

D602 Type 425, 00DD-001-001-1DG Blue cathode feed

D603 Type 425, 00DD-001-001-1DG Red cathode feed

MISCELLANEOUS

* TB61 90° CRT socket, 00F6-389-001 (110° CRT socket, 00F6-305-002)

TG61 Snap in tag 00K8-009 (Earth blade, 06B1-437-001) TG62 Earth blade, 06B1-437-001

For Service Manuals Contact MAURITRON TECHNICAL SERVICES 8 Cherry Tree Rd, Chinnor Oxon OX9 4QY Tel:- 01844-351694 Fax:- 01844-352554 Email:- enquiries@mauritron.co.uk

Diode Modulator Board (PC1153) - 110° Only

RESISTORS

R702 221kΩ 1% 0·25W, R6221-BM02-08RG Part TR72 base bias network (with R703, R712)

R703 27kΩ 5% 0·25W, R5270-GF02-01RG See R702

R704 3·3kΩ 5% 0·25W, R4330-GF02-01RG Differential amplifier emitter load

R706 39kΩ 5% 0 · 25W, R5390-GF02-01RG Part TR71 base bias (with R708)

R707 12kΩ 5% 0·25W, R5120-GF02-01RG Part of HF limiting network (with C704)

R708 8 66kΩ 1% 0 25W, R4866-BM02-08RG See R706

221kΩ 1% 0·25W, R6221-BM02-08RG

Provides negative feedback and determines gain R710 3 3kΩ 5% 0-25W, R4330-GF02-01RG

TR72 collector load 2·7Ω 5% 0·25W, R1270-GXP2-W100

TR73 emitter load R712 2·7kΩ 5% 0·25W, R4270-GF02-01RG

See R702

VARIABLE RESISTORS

RV71 1kΩ lin. 10mm preset pot., 00E1-131-410-PH1 Pincushion adjustment

RV72 4·7kΩ lin. 10mm preset pot., 00E1-131-447-PH1 Width adjustment

CAPACITORS

C701 100µF 20% 35V Elec., CE310-MS235-20CG

Field sensing coupling capacitor C702 22nF 10% 400V, C5220-SS340-RBE9

Part of diode modulator tuning network

C703 2 · 2µF 10% 100V, C7220-SS310-RF08 Line coupling C704 1nF 10% 50V, C4100-SS250-MAH3

See R707

C705 470nF 10% 160V, C6470-SS316-AR21 HT ripple sensing network

TRANSISTORS

TR71 BC309C, 00TR-006-204-1TG Half differential amplifier (with TR72) TR72 BC309C, 00TR-006-204-1TG

See TR71

TR73 TIP110, 00TR-030-801-1TG Diode modulator driver

DIODES

D701 SK4G4/04, 02V4-711-200 Part of efficiency diode network

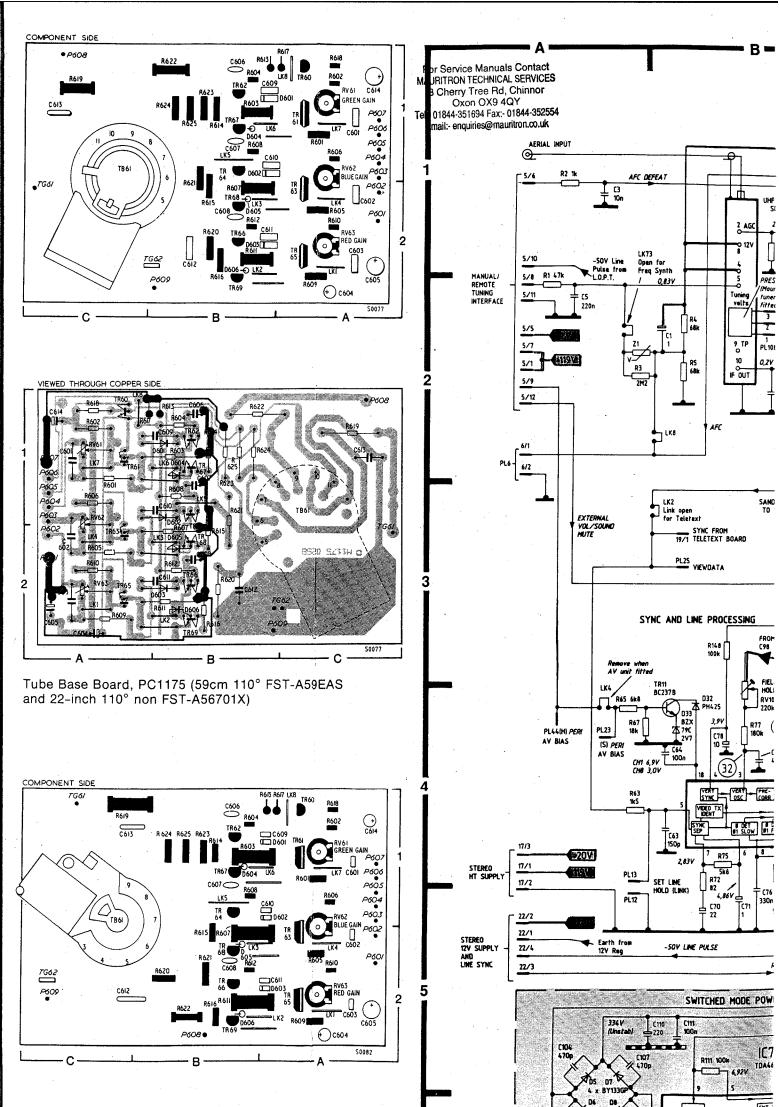
INDUCTORS

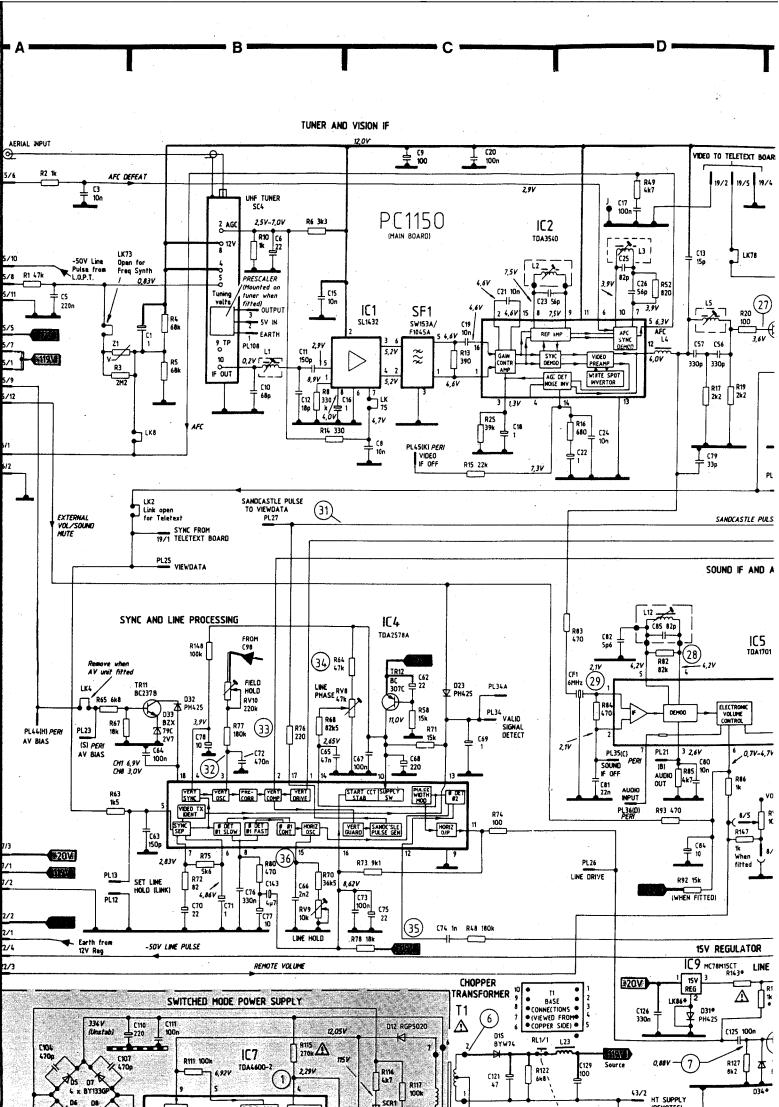
L701 Diode mod. choke, 90D4-090-001-01G Provides impedance between line stage and diode

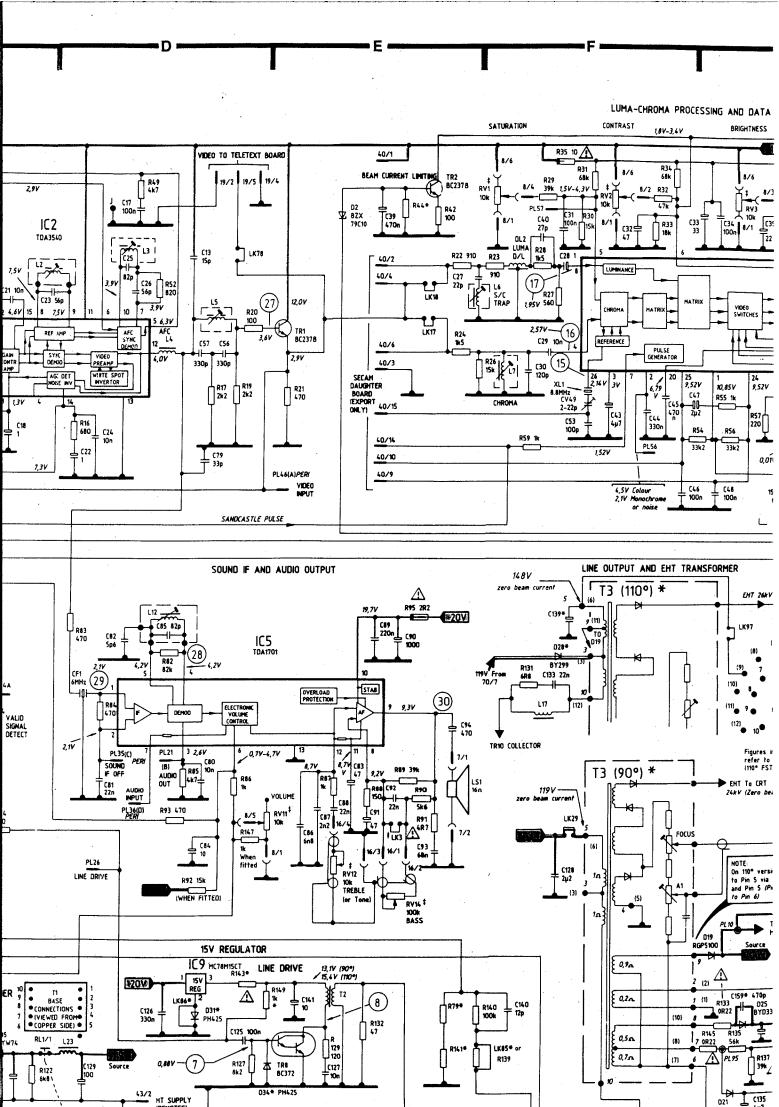
modulator Diode mod. choke, 90D4-091-001-01G Provides impedance between C703 and line tuning

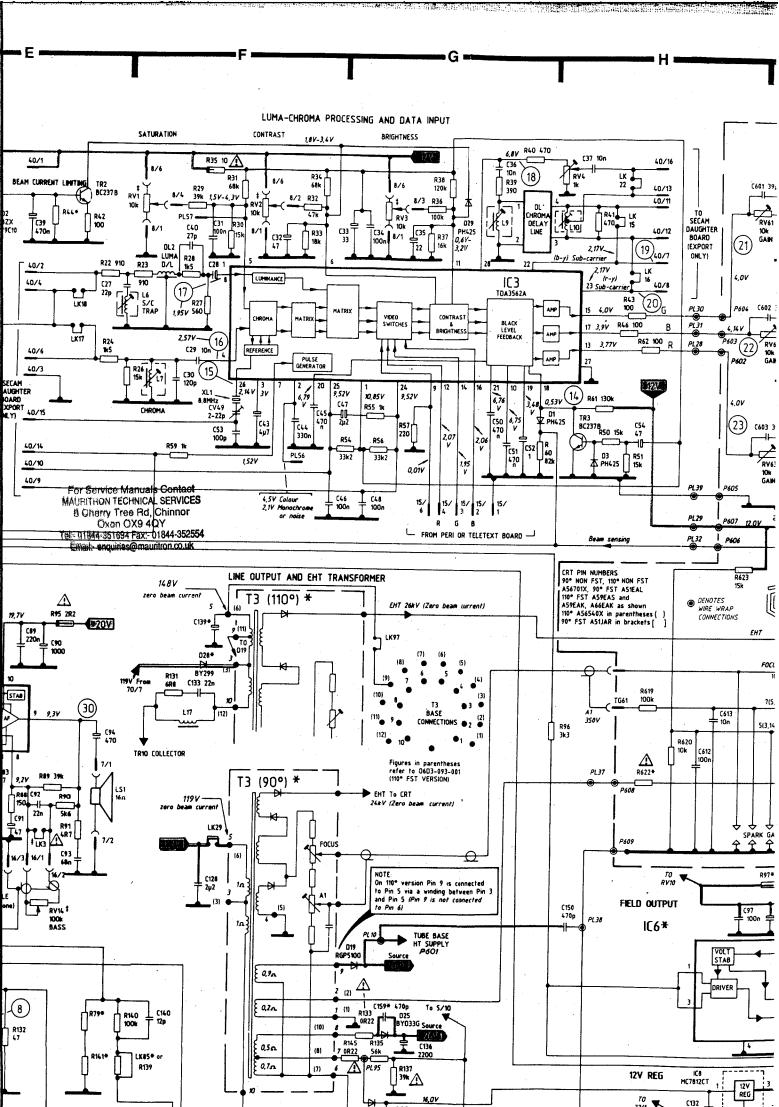
MISCELLANEOUS

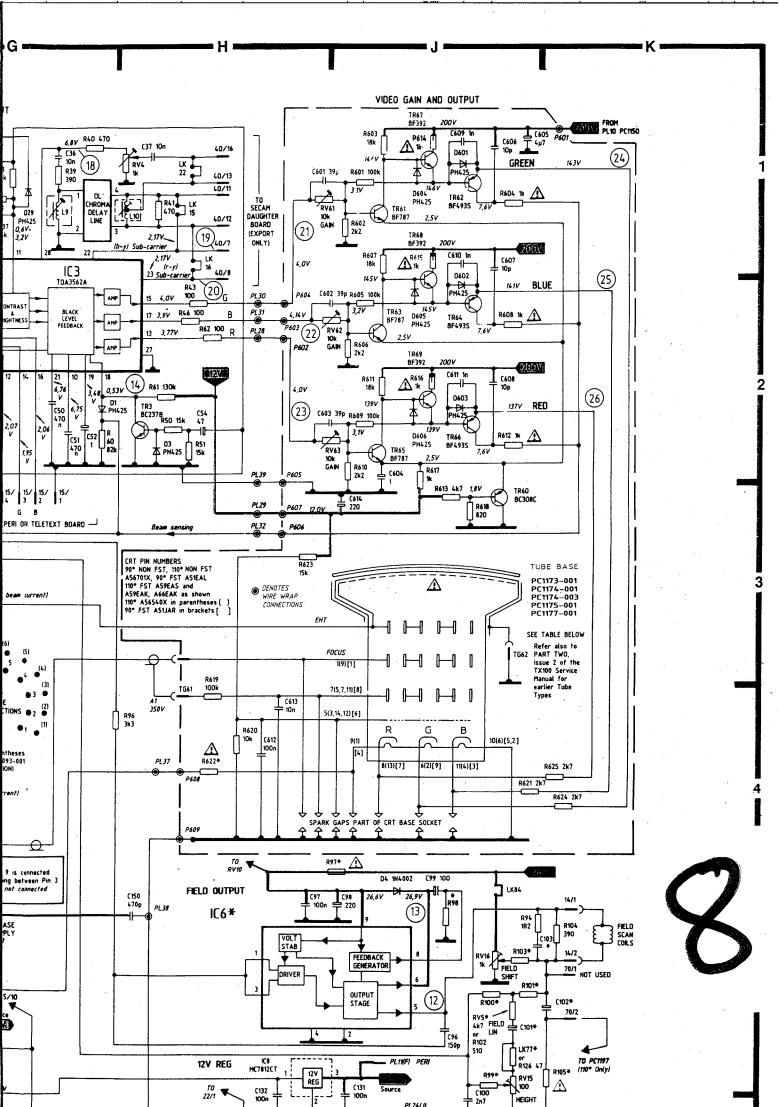
SK70 7-way edge connector, 90F6-023-005

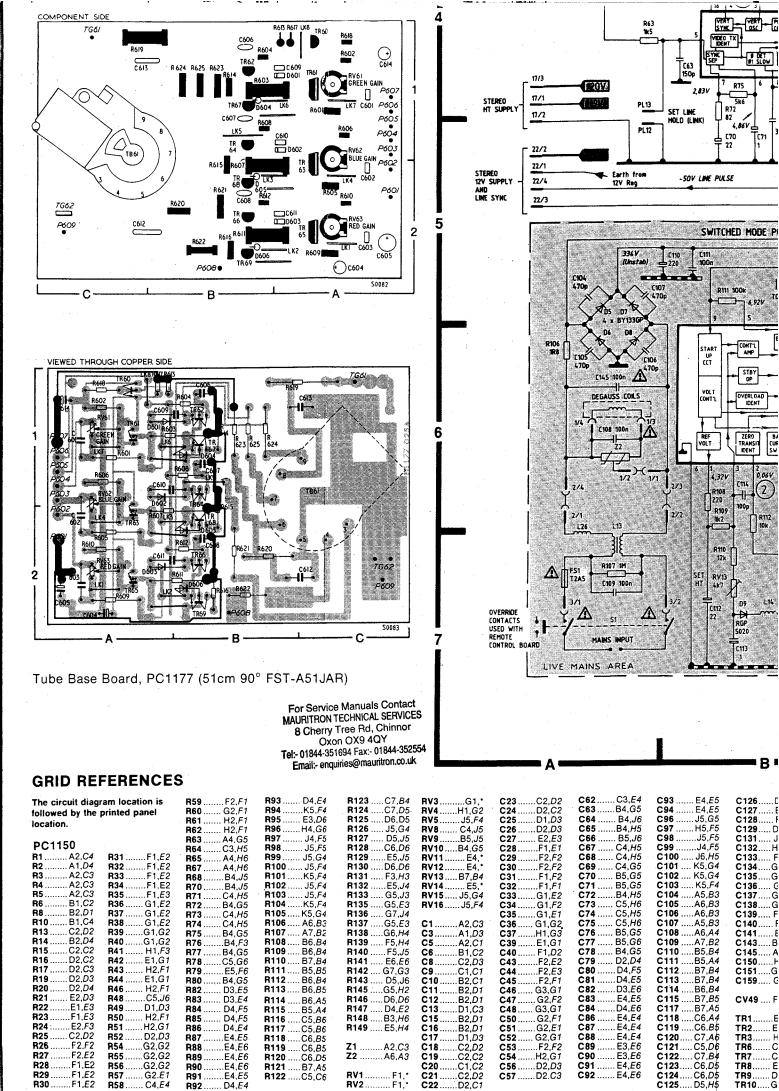


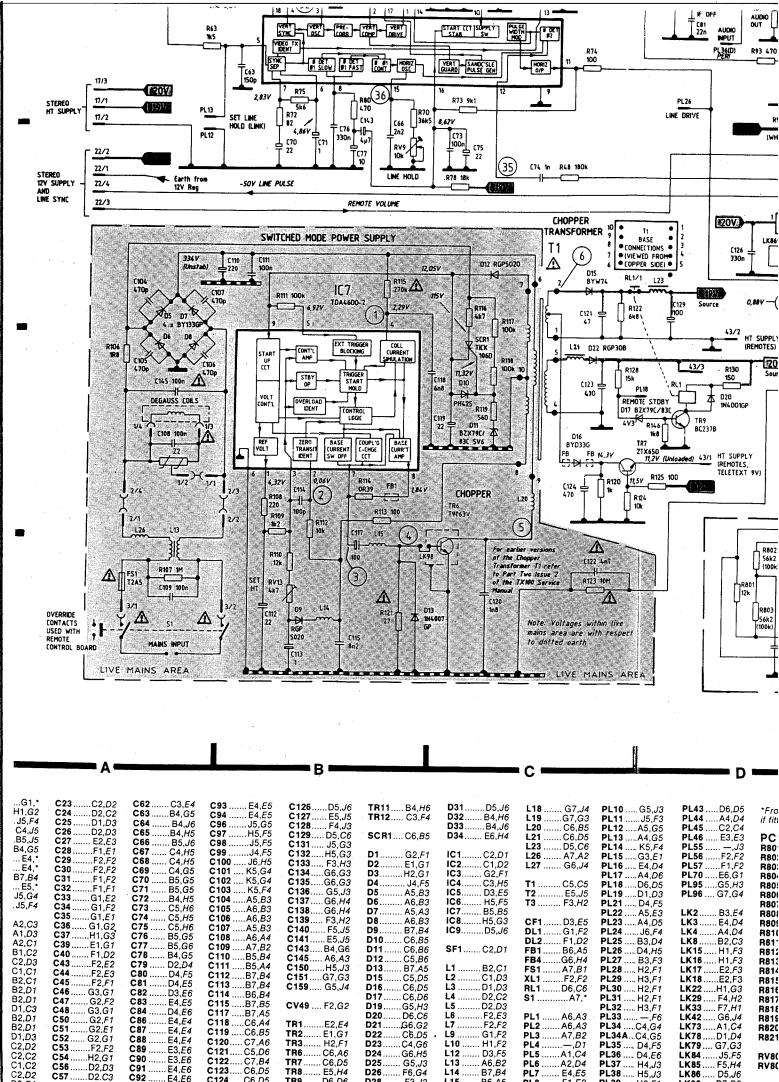












TRB

TR10.

C124..... C6,D5 C125..... D5,H5

C57 D2.C3

C92 E4,E6

F5 H4

...G6,H4

.... F6,G4 F3,J2

..... G1,E1

D26

D28

D29

L14 .

L17

B7,B4

B6,A5

F4,H3

PL7 E4,E5 PL8F1.E2

PL9

.....G6,H4

.... H5,J3

H2,F1

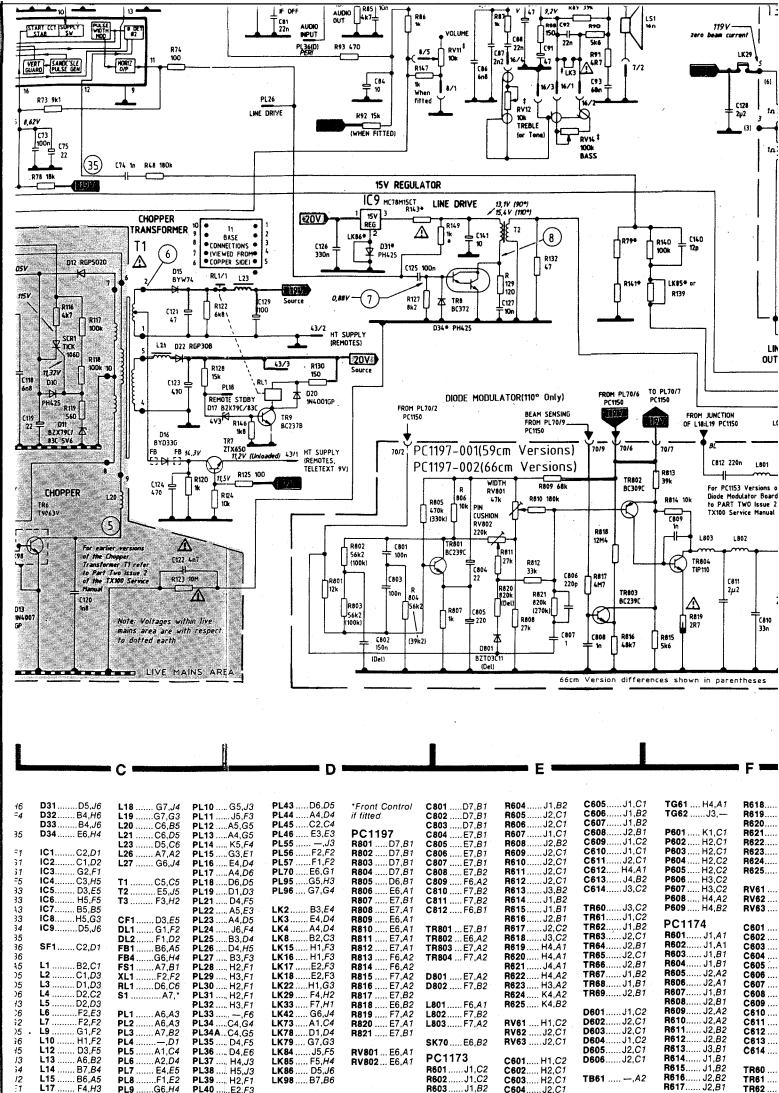
PL39

PL40.

LK86 D5,J6

.... B7,B6

LK98



R602.....J1,C2

R603..... J1,B2

C604.....J2.C1

.... H2,F1

PL40 E2,F3

B7.B6

PL39

L15

B6.A5

..... F4,H3

PI 8

PL9

.....G6,H4

R616..... J2,B2

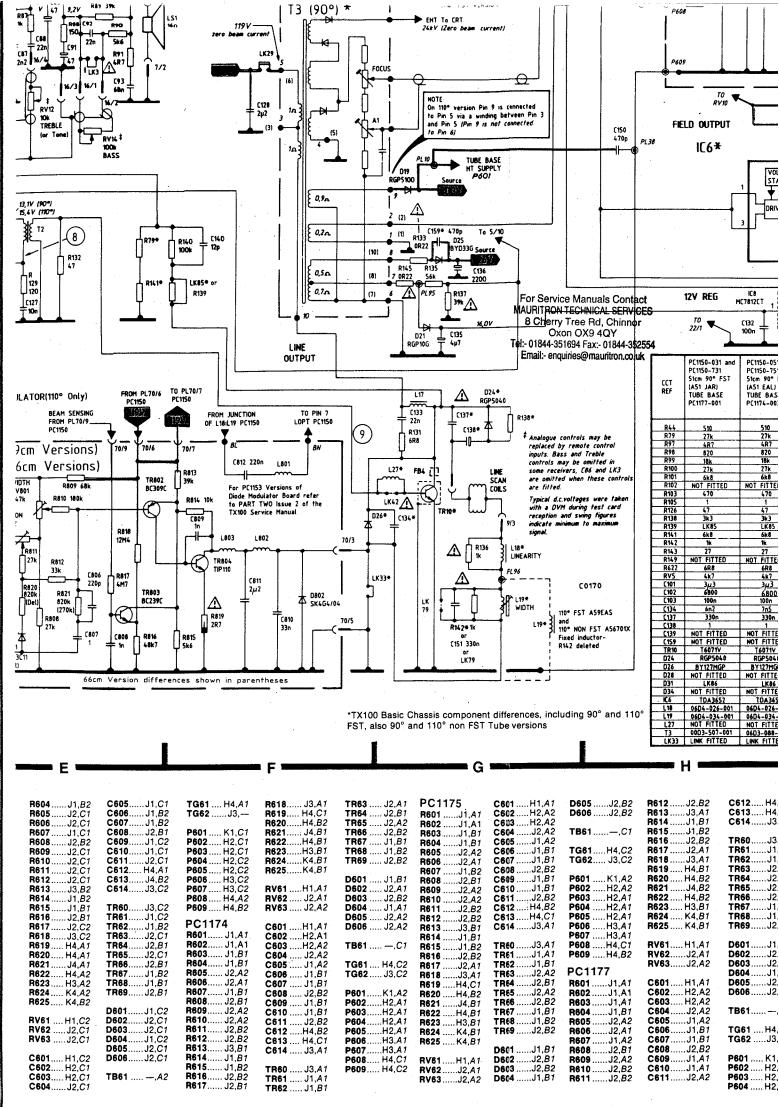
J2.B1

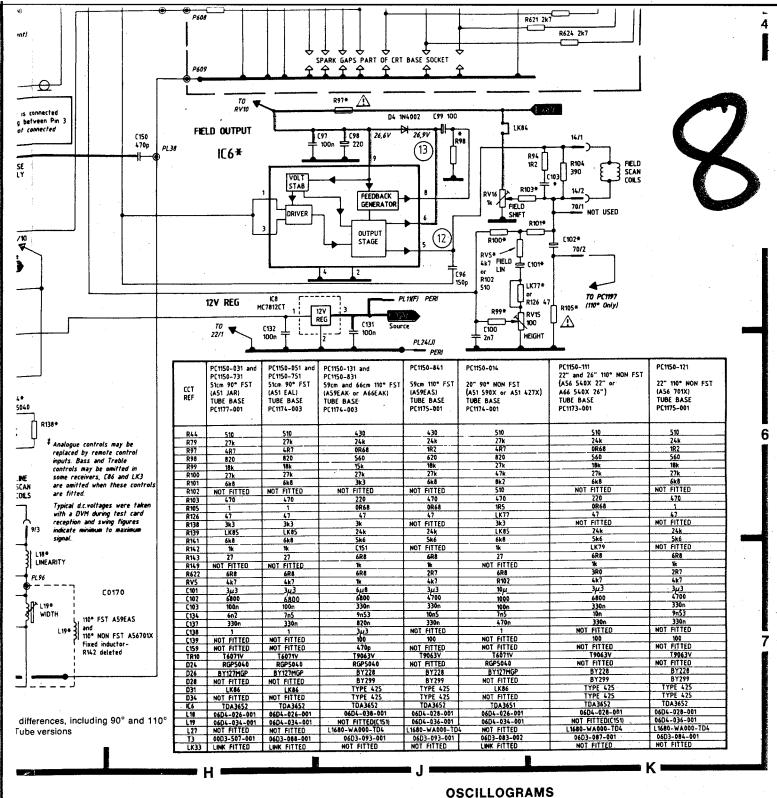
R617.

TR61

TR62

TB61 --. A2

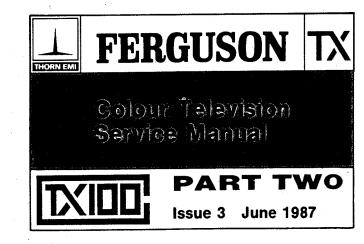




C601 H1,A1	D605J2.B2	R612 J2,B2	C612 H4,C2	P605 H2,A1
C602 H2,A2	D606J2,B2	R613 J3,A1	C613 H4,C1	P606 H3,A1
C623 H2.A2		R614 J1.B1	C614J3,A1	P607 H3,A1
C604J2,A2	TB61 C1	R615 J1.B2		P608 H4,B2
C605J1.A2	,	R616 J2.B2	TR60J3,A1	P609 H4,C2
C606J1,B1	TG61H4.C2	R617J2.A1	TR61J1,A1	
C607 J1,B1	TG62 J3.C2	R618 J3.A1	TR62J1,B1	
C608 J2,B2		R619 H4,B1	TR63J2,A2	
C609 J1,B1	P601 K1,A2	R620 H4.B2	TR64J2,B1	
C610J1,B1	P602 H2.A2	R621 J4.B2	TR65J2,A2	
C811 J2,B2	P603 H2,A1	R622 H4.B2	TR66J2,B2	
C612 H4.B2	P604 H2,A1	R623 H3,B1	TR67J1,B1	
C613 H4,C1	P605 H2,A1	R624 K4.B1	TR68J1.B2	
C614 J3,A1	P606 H3.A1	R625 K4.B1	TR69J2.B2	
	P607 H3,A1			
TR60 J3,A1	P608 H4,C1	RV61 H1,A1	D601J1.A1	
TR61 J1,A1	P609 H4,B2	RV62J2,A1	D602J2,A1	
TR62 J1,B1	·	RV63J2.A2	D603J2,A2	
TR63 J2,A2	PC1177		D604J1.B1	
TR64 J2,B1	R601 J1.A1	C601 H1.A1	D605J2.B2	
TR65 J2,A2	R602 J1,A1	C602 H2,A2	D606J2.B2	
TR66J2,B2	R603J1.A1	C603 H2,A2		
TR67 J1,B1	R604 J1.B1	C604J2.A2	TB61	
TR68J1,B2	R605 J2.A2	C605J1,A2		
TR69 J2,B2	R606 J2,A1	C606J1,B1	TG61 H4,C1	
	R607 J1.A2	C607J1,B1	TG62J3,C2	
D601J1,B1	R608 J2.B1	C608J2.B2		
D602J2,B1	R609 J2.A2	C609J1,A1	P601 K1,A1	
D603J2,B2	R610 J2,B2	C610J1,A1	P602 H2,A1	
D604J1,B1	R611 J2,B2	C611J2,A2	P603 H2,A1	02P1-844-018
			P604 H2,A1	(Part of 02P1-844)

The trace pictures were taken from a typical receiver at the points indicated by encircled numbers.

The oscillograms are shown in PART TWO Issue 1 of the TX100 Service Manual.



INSTALLATION and ACCESS FOR SERVICE

SAFETY COVER

As indicated on the circuit diagram an area of the main printed circuit board, PC1150, carries live mains. This area is protected by a moulded plastic cover, which should not be removed unless absolutely necessary. Adequate precautions must be taken when servicing in this area.

Mains Connection

The receiver operates from a.c. mains supplies 185V-265V 50Hz. No input adjustment is required.

The chassis is isolated. As indicated on the top printing, an area of the printed circuit board carries live mains and this is protected above and below by plastic covers which should not be removed unless absolutely necessary.

Fuse

FS1 mains input T2A5 (20mm cartridge type).

Degaussing

The built-in degaussing circuit operates whenever the receiver is switched on from cold, neutralizing all but the most severe cases of magnetization.

On installation, the receiver may be manually degaussed with an external coil should this be considered necessary.

Aerial

A wide bandwidth aerial is required and careful siting and orientation are necessary for the best signal strength with freedom from ghosting on all available channels. This is particularly important when installing a receiver fitted with teletext facilities. Low-loss 75Ω coaxial feeder should be used.

Automatic Inter-Station Muting

When switched on with the aerial disconnected, or if the receiver is not tuned into a station with the aerial connected, the usual background noise is automatically silenced. There is, therefore, no background noise between stations during the tuning-in procedure.

Removing Cabinet Back

The cabinet back moulding hooks into slots in the cabinet base, and is held at the top by either plastic screws or a simple barb and catch arrangement. Press down on the barb whilst pulling the top of the back away from the cabinet. Swing back the top to free the back moulding from the slots in the cabinet base.

Chassis Removal

The chassis frame is positioned in the bottom of the cabinet by lugs on either side of the frame which locate in slots at the bottom of the cabinet. The chassis is latched into the cabinet base by a lip on each of the rear lugs.

On certain models the chassis is further secured to the cabinet base by the addition of three or four screws. It is important to replace these screws if they are removed during servicing.

To remove the chassis, unscrew the securing screws (if fitted) and lift the right-hand side rear of the chassis frame in order to detach it. With the other hand, push the right-hand side front of the chassis frame towards the rear of the cabinet; refer to diagram. Repeat this procedure with the left-hand side of the chassis frame after which the chassis may be removed or fitted into the servicing position.



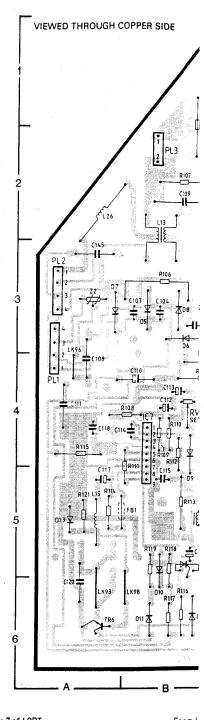
Removing Chassis from Cabinet

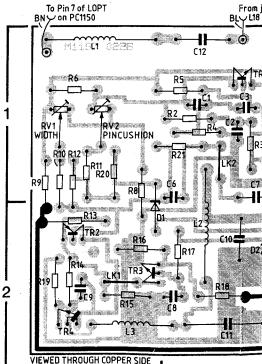
Chassis Servicing Position

The chassis may be fitted into a sloping position to enable the printed circuit board to be easily serviced whilst in an operational mode, both component and copper sides being accessible. The two protruding lugs at the front of the chassis frame slot into the cabinet base.

Component Differences for the 66cm Version of PC1197-(002)

R802	100k 5%
R803	100k 5%
R804	39.2k 1%
R805	330k 5%
R821	270k 5%
R820	Deleted
C802	Deleted





SEMICONDUCTOR BASES

ERVICE

Back

hooks into
d is held at
ews or a
ngement.
elst pulling
m the
to free the
ts in the

ned in the s on either te in slots at he chassis is e by a lip on

sis is further by the ews. It is crews if they g.

rew the d lift the hassis With the and side wards the diagram. he left-hand er which the fitted into



Cabinet

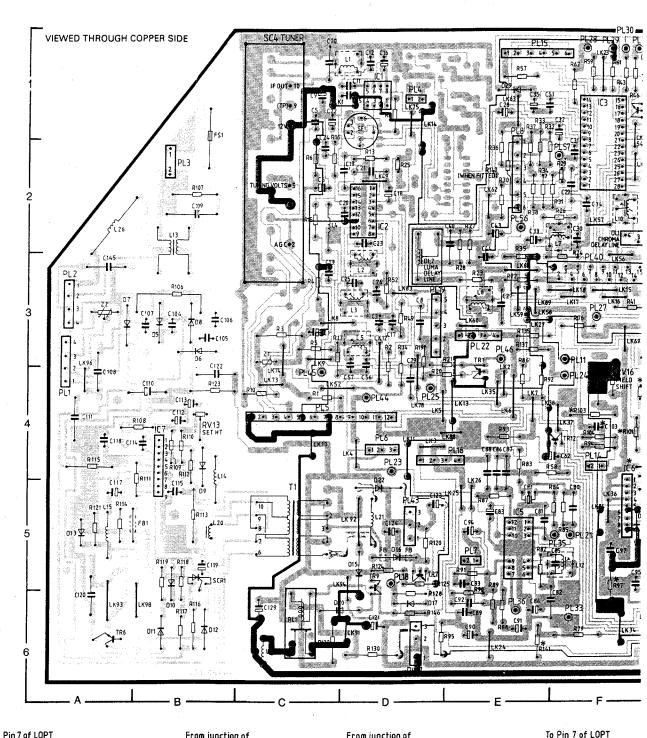
o a sloping circuit hilst in an conent and . The two the chassis

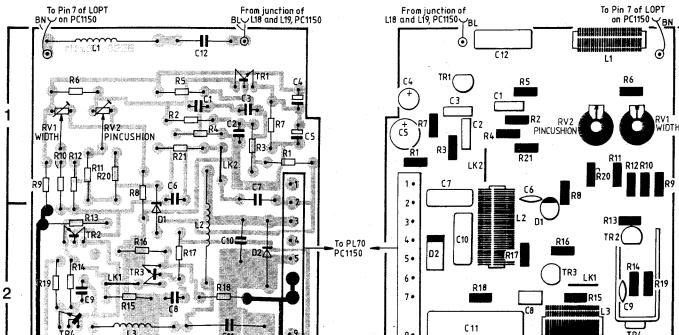
ences for ersion of 197-(002)

.... 100k 5% 100k 5% 39.2k 1% 330k 5%

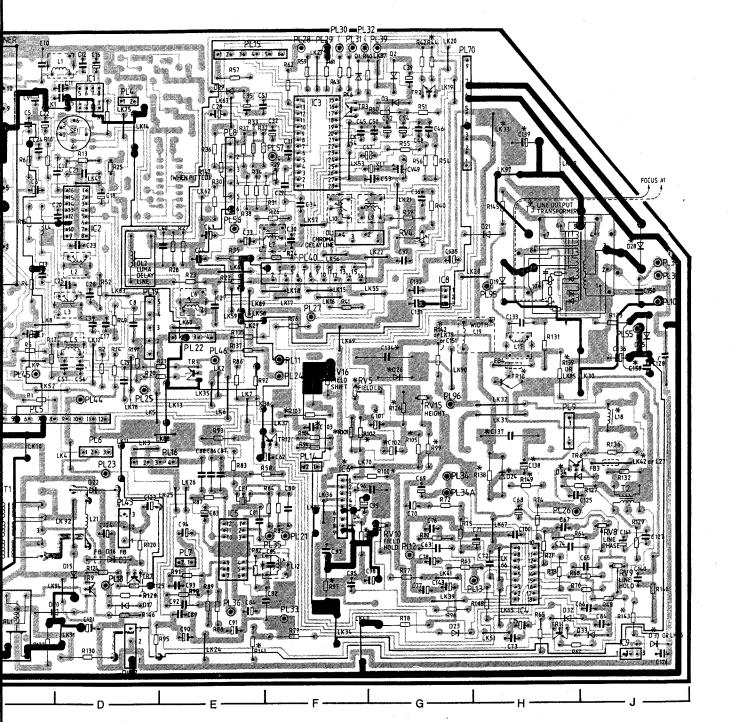
.... 270k 5% Deleted

..... Deleted





SK70



Main Board, PC1150 (*all versions)

*Component differences for various versions of the Main Board PC1150 are shown in the table overleaf

SERVICING ADJUSTMENTS

Full adjustment procedures, some of which may require the use of an oscilloscope etc; are given in the Main Chassis information section.

WARNING

EHT Shock Hazard

The EHT must be safely discharged before attempting to disconnect the EHT lead from the tube anode.

Clip one end of a convenient lead, such as a meter lead, to the tube earthing strap on the tube body, fold back the suction can and discharge the EHT

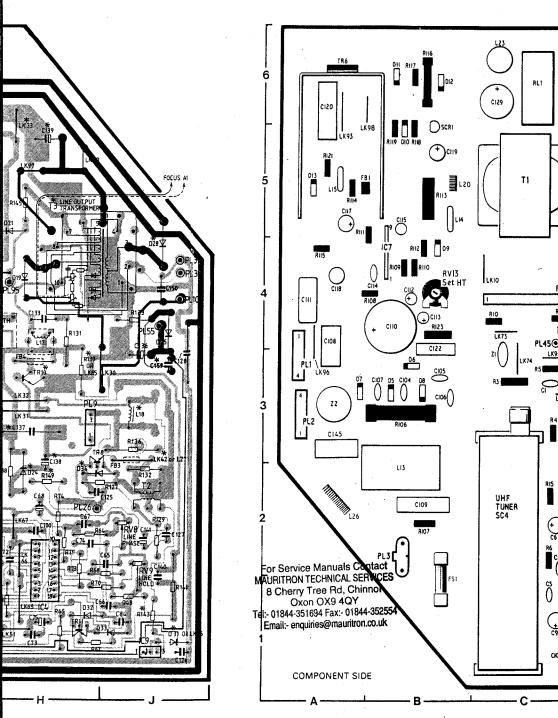
Field Linearity (

Adjust RV5 for b top and bottom

Line linearity is f

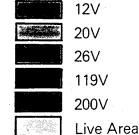
Picture Shift (R

Adjust Line Phas RV16 to centre t



€)¢3I LK83 ()cız

rd, PC1150 (*all versions) ent differences for various versions of the d PC1150 are shown in the table overleaf



indicates critical safety components, and identical components should be used for replacement.

ICING ADJUSTMENTS

ent procedures, some of which may require the use of an etc; are given in the Main Chassis information section.

NG

Hazard

st be safely discharged npting to disconnect the EHT e tube anode.

d of a convenient lead, such ead, to the tube earthing tube body, fold back the and discharge the EHT

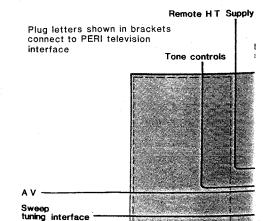
Field Linearity (RV5)

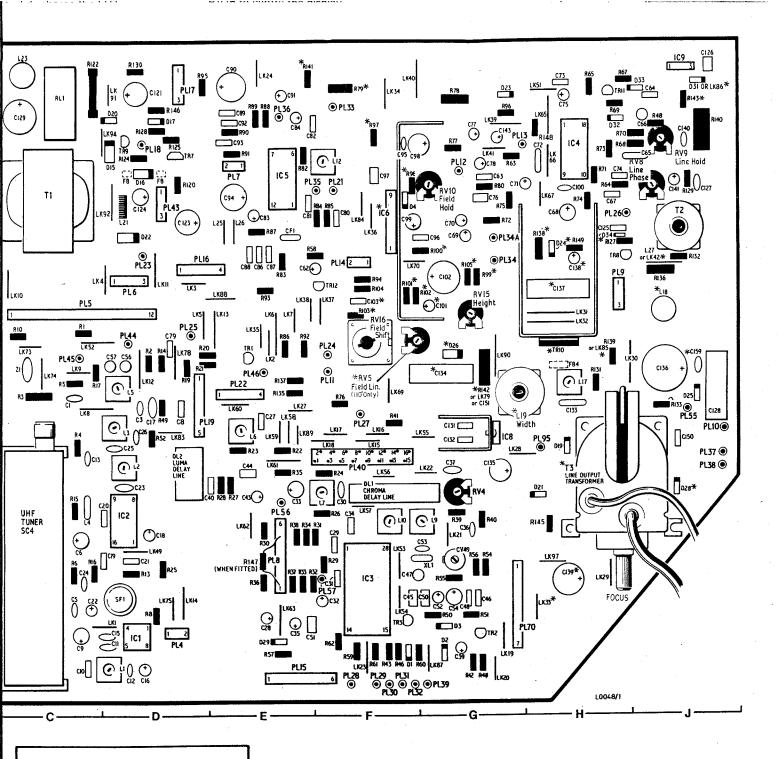
Adjust RV5 for best field linearity at the top and bottom of the display.

Line linearity is fixed.

Picture Shift (RV8 and RV16)

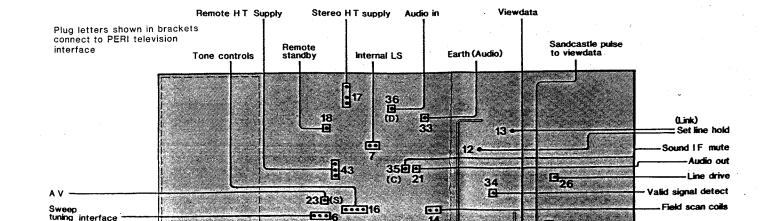
Adjust Line Phase RV8, and Field Shift RV16 to centre the display.





indicates critical safety components, and identical components should be used for replacement.

MAIN CHASSIS PLUG IDENTIFICATION

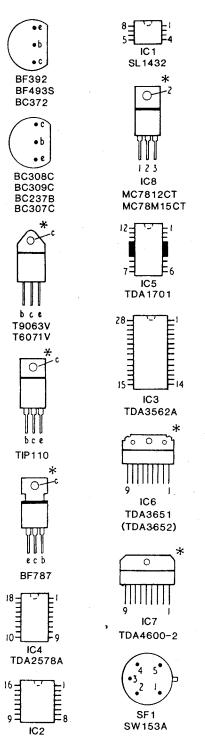


Automatic Inter-Station Muting

When switched on with the aerial disconnected, or if the receiver is not tuned into a station with the aerial connected, the usual background noise is automatically silenced. There is, therefore, no background noise between stations during the tuning-in procedure.

SEMICONDUCTOR BASES

ALL BASES EXCEPT * VIEWED FROM UNDERSIDE

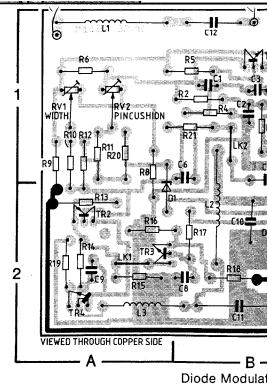


Chassis Servicing Position

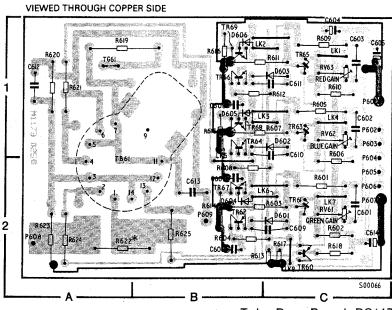
The chassis may be fitted into a sloping position to enable the printed circuit board to be easily serviced whilst in an operational mode, both component and copper sides being accessible. The two protruding lugs at the front of the chassis frame slot into the cabinet base.

Component Differences for the 66cm Version of PC1197-(002)

	100k 5% 100k 5%	
R804	39.2k 1%	
R805	330k 5%	
R821	270k 5%	
C802	Deleted Deleted Deleted	

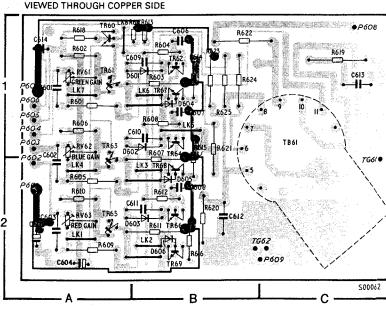


and PC1197-0

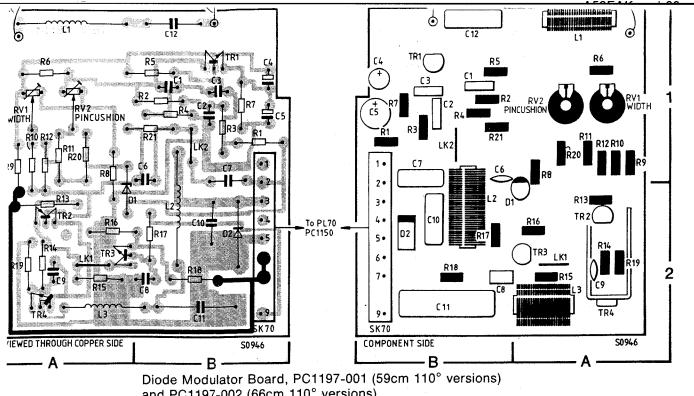


Tube Base Board, PC117 and 26-inch 110° non FS

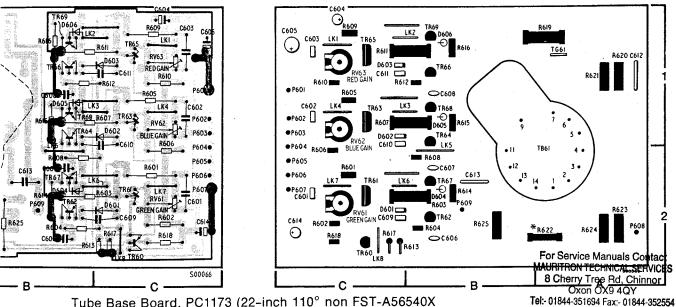
VIEWED THROUGH COPPER SIDE



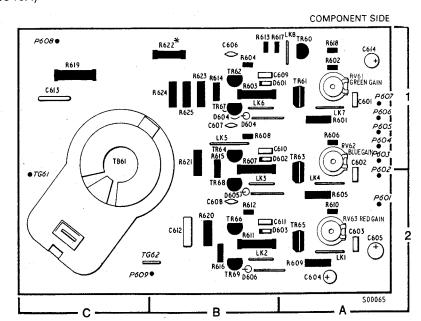
Tube Base Board, PC1174-001 and A51427X) PC1174-003 (51 A59FAK and 66cm 110° FST-A



and PC1197-002 (66cm 110° versions)



Tube Base Board, PC1173 (22-inch 110° non FST-A56540X and 26-inch 110° non FST-A66540X)



Tube Base Board, PC1174-001 (20-inch 90° non FST-A51590X and A51427X) PC1174-003 (51cm 90° FST-A51EAL, 59cm 110° FST-A59FAK and 66cm 110° FST-A66FAK)

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COMPONENT SIDE

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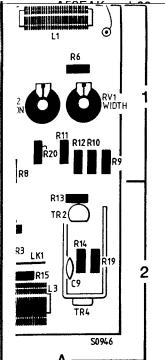
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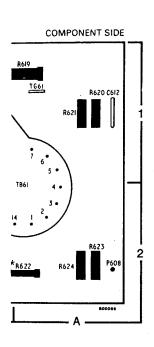
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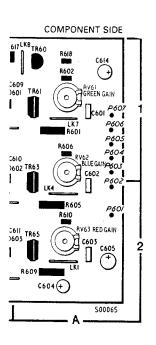
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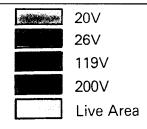
Adjus edges







Main Board PC1150 are shown in the table overleaf



SERVICING ADJUSTMENTS

Full adjustment procedures, some of which may require the use of an oscilloscope etc; are given in the Main Chassis information section.

WARNING

EHT Shock Hazard

The EHT must be safely discharged before attempting to disconnect the EHT lead from the tube anode.

Clip one end of a convenient lead, such as a meter lead, to the tube earthing strap on the tube body, fold back the suction cap and discharge the EHT through the lead.

Press in one side of the spring clip which projects into the tube cavity to ease removal of the EHT connector.

IMPORTANT

Do not disturb the tube neck adjustments as these have been set for optimum performance during tube manufacture.

Before attempting the following adjustments the receiver should be tuned if possible to a test card with the brightness, contrast and colour controls adjusted for the best picture, unless stated otherwise.

Receivers fitted with remote facilities should be normalized by switching off and on again before adjusting the preset controls. On certain receivers some of the analogue controls, i.e., brightness, contrast etc., may be presets on the remote control receiver board.

The adjustments should be carried out in the following order for convenience.

Set HT (RV13)

Turn contrast and brightness controls to minimum for zero beam current. Check voltage at pin 5 of LOPT with a $20k\Omega/volt$ meter of 2% accuracy. If necessary, adjust RV13 for 119V (90° tube) or 148V (110° tube). Adjust contrast and brightness for best picture.

Picture Geometry

Line Hold (RV9)

Link PL12 and PL13 together. Adjust RV9 for the best floating but resolved display attainable. The display will lock when the link is removed.

Field Hold (RV10)

Starting with RV10 fully counterclockwise, adjust for a steady picture and note the position. Continue rotation until the picture suddenly increases in height. Then back off until approximately half way between these two positions.

Pincushion (RV802-110° only)

Adjust RV802 for straight verticals at the edges of the display.

Field Linearity (RV5)

Adjust RV5 for best field linearity at the top and bottom of the display.

Line linearity is fixed.

Picture Shift (RV8 and RV16)

Adjust Line Phase RV8, and Field Shift RV16 to centre the display.

Picture Size (L19, RV15 and RV801)

Adjust Height control RV15 in conjunction with Width control L19 for 90° or RV801 for 110°, for full scan consistent with a correctly proportional display.

Focus

Adjust for optimum overall resolution.

Grey Scaling Procedure

Video Output Gain (RV61, RV62 and RV63)

Ensure that the three video output gain presets RV61, RV62 and RV63 are set to mid position.

Highlights Final Adjustment

With a suitable picture displayed inspect the highlights for colouration.

If green, turn down RV61.

If red, turn down RV63.

IMPORTANT: Do not readjust the blue output gain preset RV62. If highlights are blue, turn up red and green presets.

A1 Preset

With a normal picture displayed, ensure that the A1 preset is at mid position. Rotate the A1 preset clockwise until the picture begins to lose contrast and note the position of the screwdriver slot.

Rotate the A1 preset counter-clockwise until the picture again begins to lose contrast or loses one colour, and note the position of the screwdriver slot. The approximate position of the A1 preset should be midway between the two noted positions of the screwdriver slot.

4-43MHz Chroma Trap (L6)

Adjust L6 for minimum chroma patterning on the picture with the colour control at minimum.

Chroma Input Filter (L7)

Measure the d.c. volts on pin 2 of IC3.
Display a locked colour picture and adjust
L7 for maximum d.c.

NOTE: The meter must not load pin 2 appreciably.

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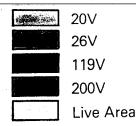
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indicates critical safety components, and identical components should be used for replacement.

MAIN CHASSI

MENTS

ay require the use of an information section.

Field Linearity (RV5)

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Line linearity is fixed.

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Picture Size (L19, RV15 and RV801)

Adjust Height control RV15 in conjunction with Width control L19 for 90° or RV801 for 110°, for full scan consistent with a correctly proportional display.

Focus

Adjust for optimum overall resolution.

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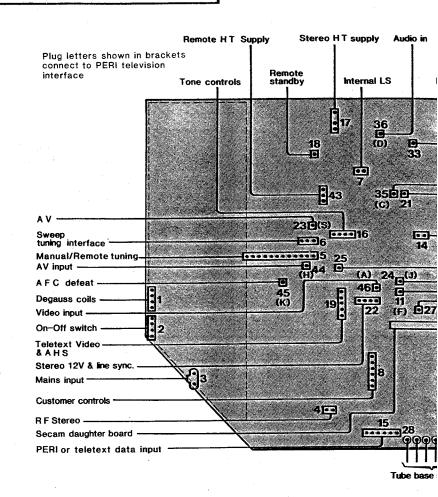
4.43MHz Chroma Trap (L6)

Adjust L6 for minimum chroma patterning on the picture with the colour control at minimum.

Chroma Input Filter (L7)

Measure the d.c. volts on pin 2 of IC3. Display a locked colour picture and adjust L7 for maximum d.c.

NOTE: The meter must not load pin 2 appreciably.



Many of these plugs are only used in certain specifications such as Remote Con

Chrominance Adjustments

The following setting up adjustments are carried out with the receiver operated from an off-air colour bar signal or UHF colour bar generator connected to the aerial socket.

Set the customer controls as follows: brightness to the centre of its range, contrast and colour to approximately two-thirds of their maximum setting.

Subcarrier Oscillator (CV49)

Short circuit R31 in order to override the colour killer and colour control. Whilst looking at a colour picture, attenuate the aerial signal. Using a non-metallic trimming tool, adjust the trimmer CV49 to achieve colour lock on the weakest signal possible, occasionally interrupting the signal in order to indicate correct colour pull-in.

Reconnect the aerial and disconnect the short circuit.

Alternatively:

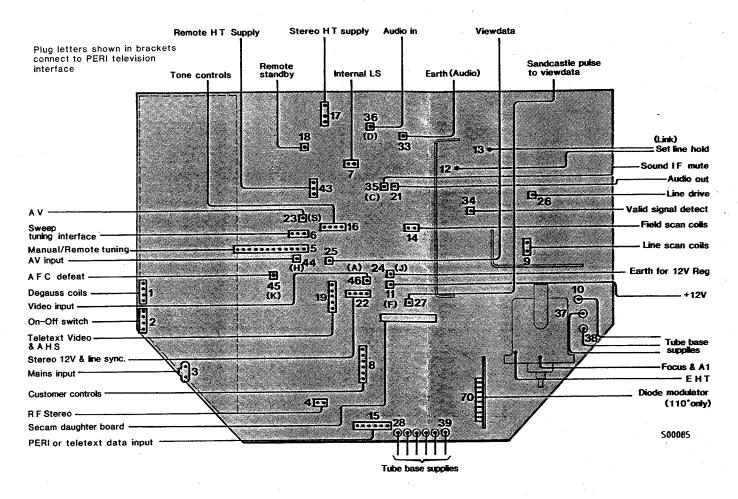
Short circuit R31 and link pins 24 and 25 of IC3 together. Using a non-metallic trimming tool adjust CV49 for zero frequency run through. Remove the links.

Chroma Delay Line Termination (RV4, L9 and L10)

Set L10 core one and a half turns dow from the top of the former and adjust RV4 and L9 for minimum venetian blin effect. In a very few cases balance ma be unattainable by adjustment of L9. If so, adjust L9 for the best setting and to L10 for balance.

indicates critical safety components, and identical components should be used for replacement.

MAIN CHASSIS PLUG IDENTIFICATION



Many of these plugs are only used in certain specifications such as Remote Control, Teletext, Sweep-Tune etc.

hrominance Adjustments

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For Service Manuals Contact
MAURITRON TECHNICAL SERVICES
8 Cherry Tree Rd, Chinnor
Oxon OX9 4QY
Tel:- 01844-351694 Fax:- 01844-35254
Email:- enquiries@mauritron.co.uk

SERVICING NOTES

Please observe the usual precautions for handling ICs and removing components from the PCB (see servicing notes in Main Chassis information section).

Replacing chopper and line output transistors TR6 and TR10. These transistors are mounted on heatsinks. The transistors are secured to the heatsinks by spring clips. To remove the clip, simply press it out from the inside of the heatsink. It is not necessary to remove the heatsink from the PCB.

Before replacing the transistors, inspect the insulating washers and replace if necessary. Secure the transistors to the heatsink by pressing the spring clip firmly in position.

Replacing ICs Mounted on Heatsinks. In the majority of cases, when replacing the ICs that are mounted on heatsinks, it is easier to remove both the heatsink and IC from the PCB, then remove the IC from the heatsink. Before replacing the IC, clean off the old heatsink compound from the heatsink and insulating washer (if fitted), and apply fresh compound to both sides. Always ensure the IC retaining screw is secured tightly.



Receivers fitted with:
Tuning and Analogue Control Systems (TACS)
Including:

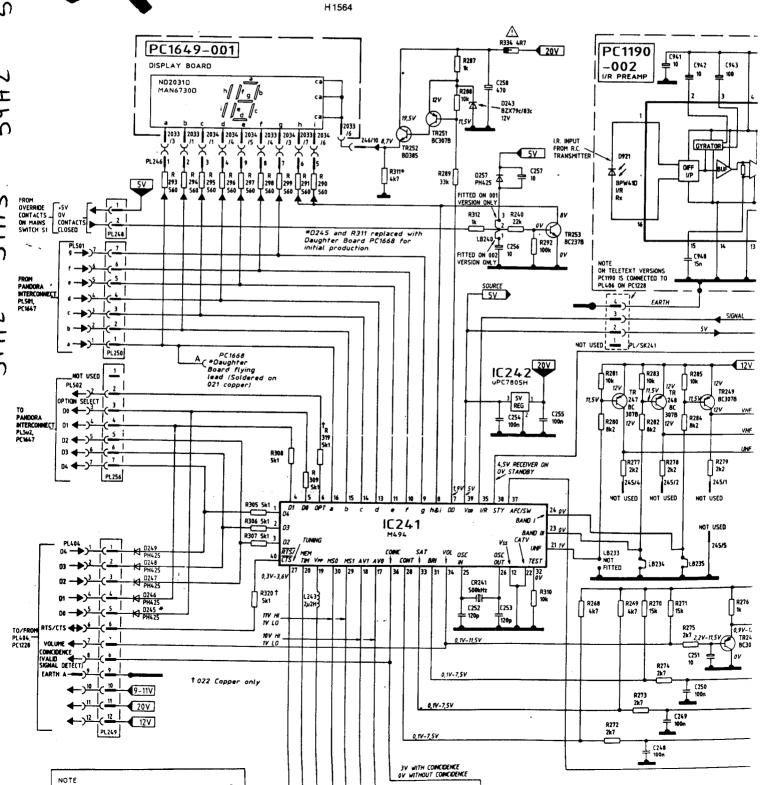
Models 51H2 and 59H2

TACS with Remote Control

Using T780 Remote Control Transmitter

Models 51H3, 59H3 and 66H3

TACS with Remote Control and FASTEXT Using T785 Remote Control Transmitter



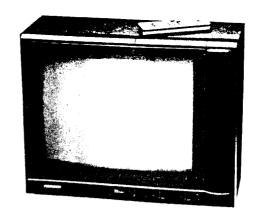
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Including:

Models 51H2 and 59H2

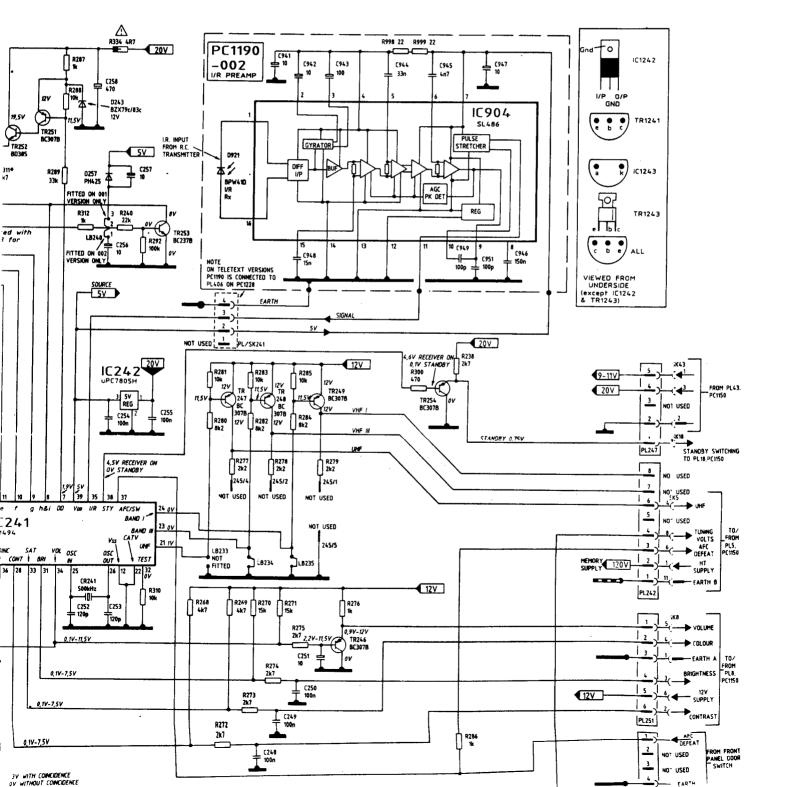
TACS with Remote Control
Using T780 Remote Control Transmitter

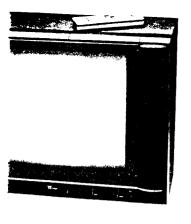
Models 51H3, 59H3 and 66H3

TACS with Remote Control and FASTEXT Using T785 Remote Control Transmitter

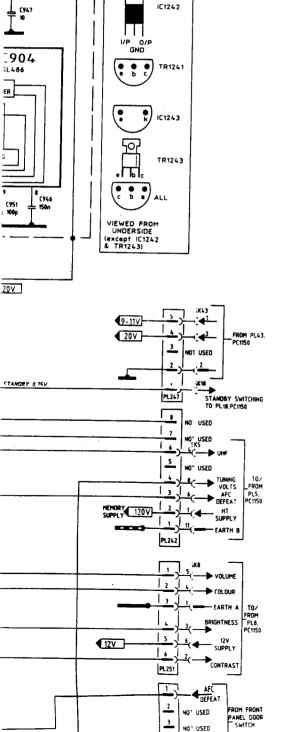


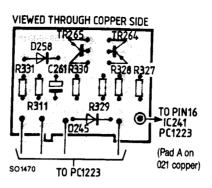
Typical TX100 Series Receiver (Model 51H3) incorporating TACS, Remote Control and FASTEXT.



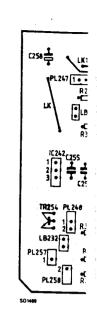


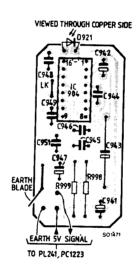
ies Receiver (Model 51H3) S, Remote Control and FASTEXT.





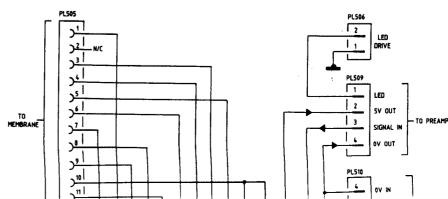
Anti-LED Off Board PC1668
(Fitted on all models) Component Layout

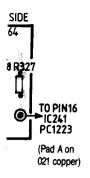




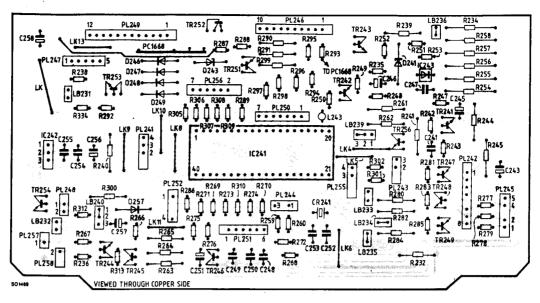
Infra-red Preamplifier PC1190-002 (Fitted on all models) Component Layout

For Service Manuals Contact
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8 Cherry Tree Rd, Chinnor
Oxon OX9 4QY
Tel: 01844-351694 Fax: 01844-352554
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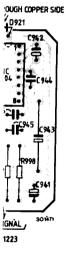




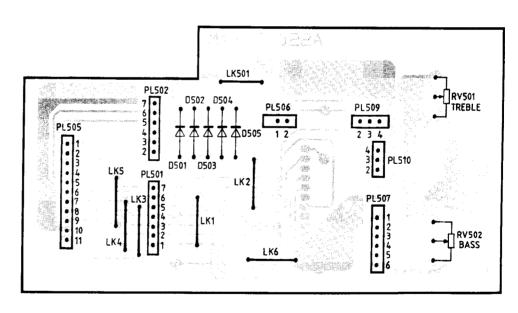
1668 omponent Layout



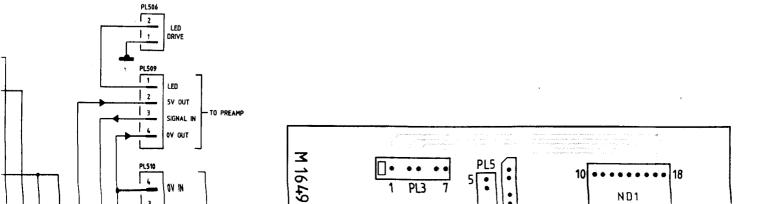
TACS Control Board PC1223-002 (Fitted on all models) Component Layout shown to 021 copper standard



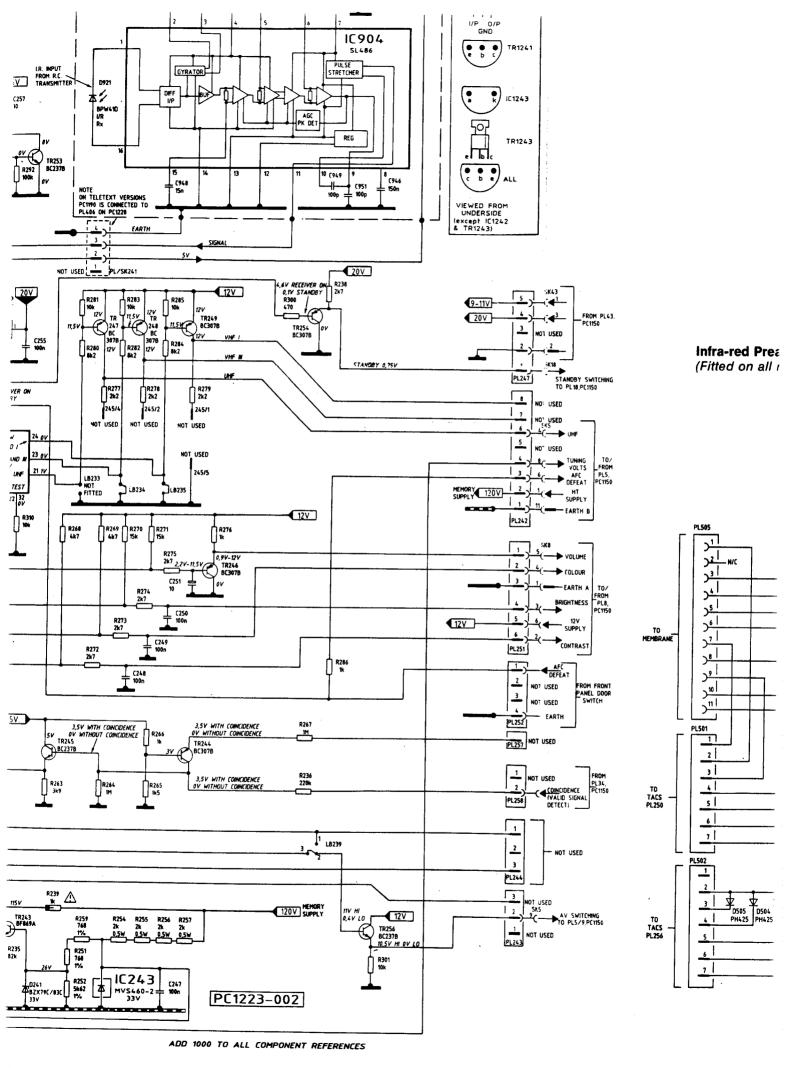
C1190-002 mponent Layout



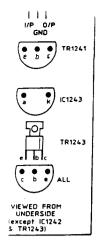
Control Interface PC1647-002 Component Location Diagram

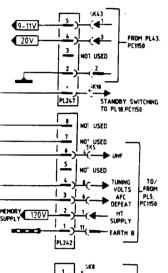


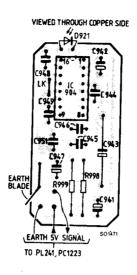
TACS Control Board PC1223-002, Anti-LED off PC1668, Channel Display Board PC1649-001 and Infra-Red Preamplifier Board PC1190-002 (All models)



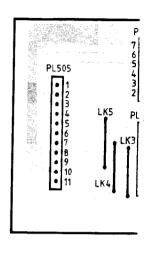
1 PC1668, Red Preamplifier Board PC1190-002





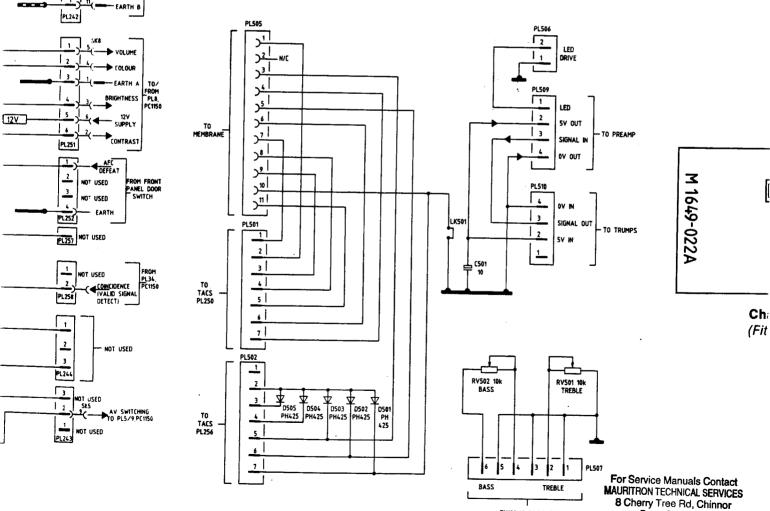


Infra-red Preamplifier PC1190-002 (Fitted on all models) Component Layout



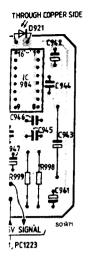
Oxon OX9 4QY

Tel:- 01844-351694 Fax:- 01844-352554 Email:- enquiries@mauritron.co.uk Cc PC

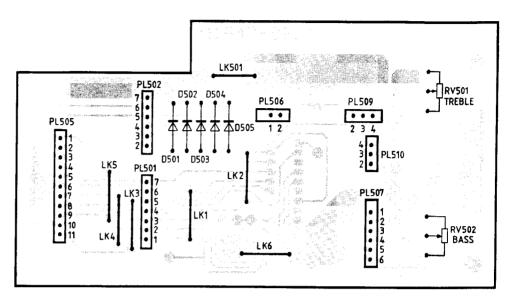


Control Interface Board PC1647-002

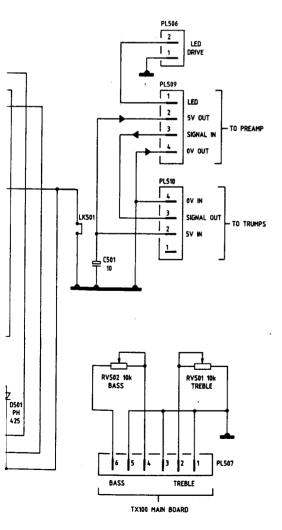
TX100 MAIN BOARD

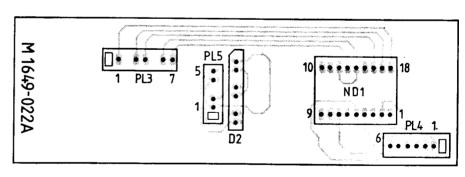


PC1190-002 Component Layout

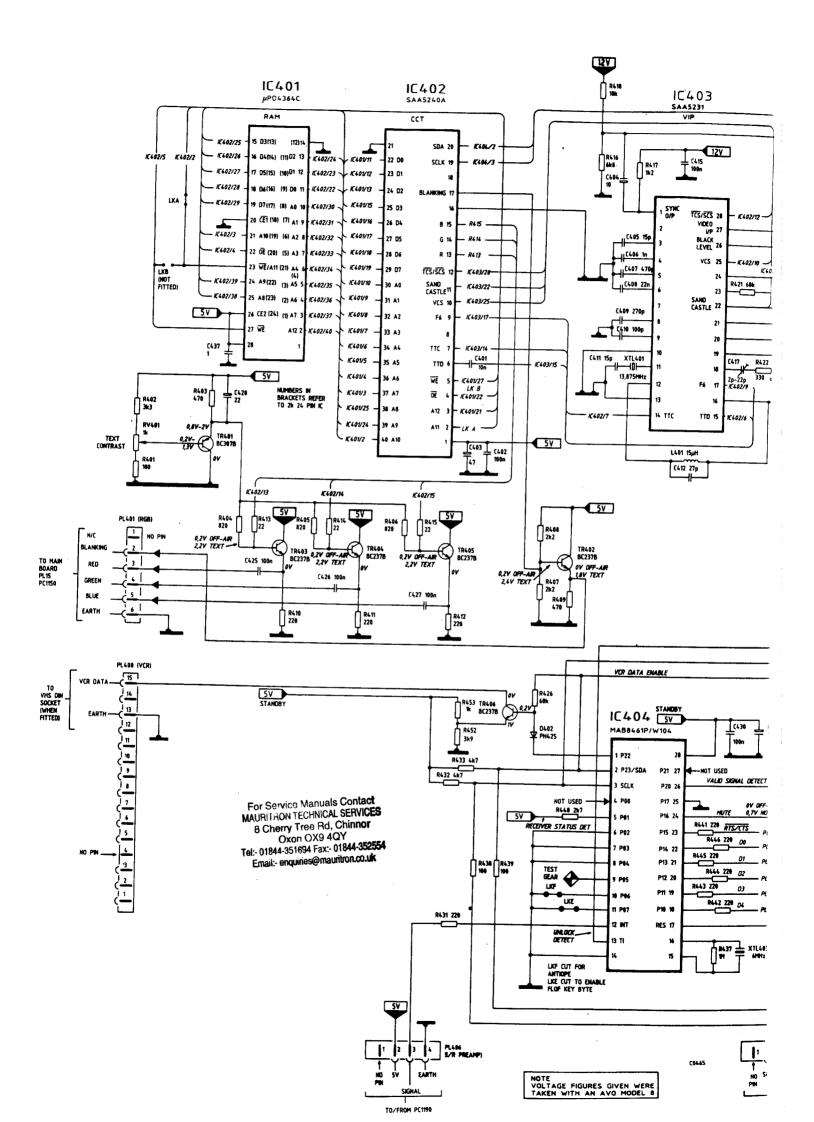


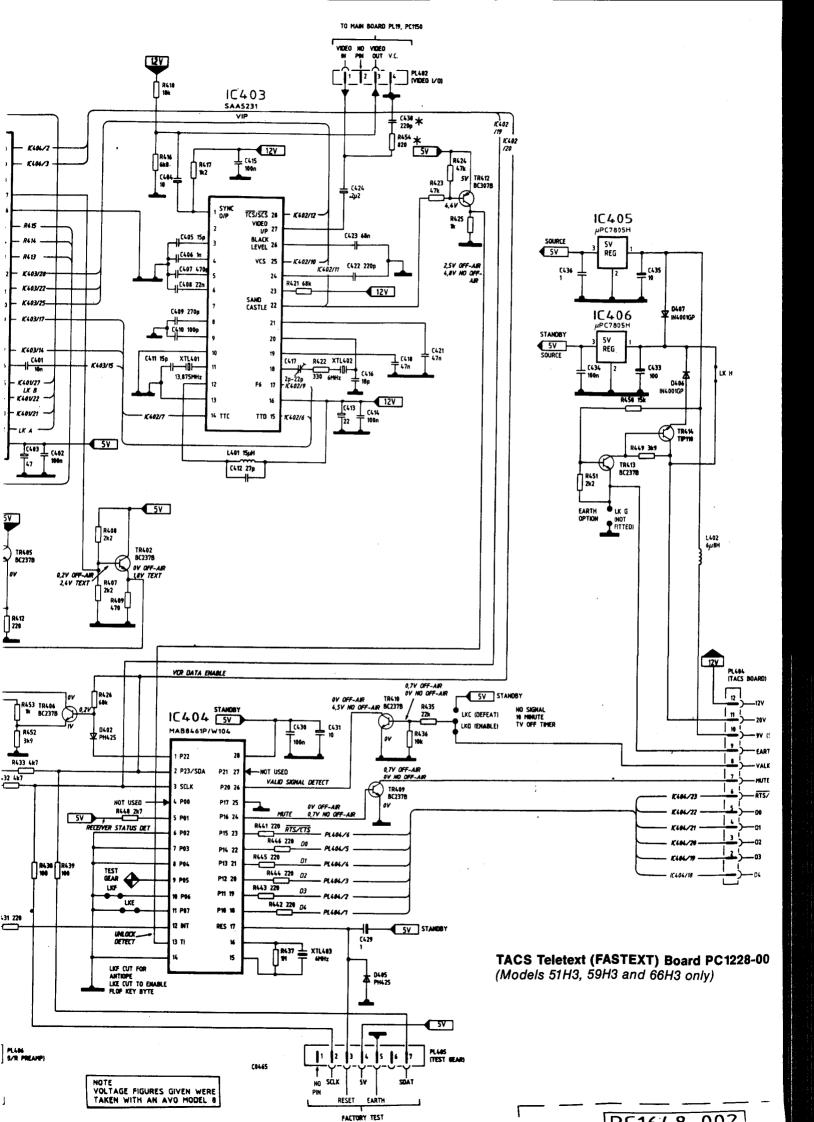
Control Interface PC1647-002 Component Location Diagram

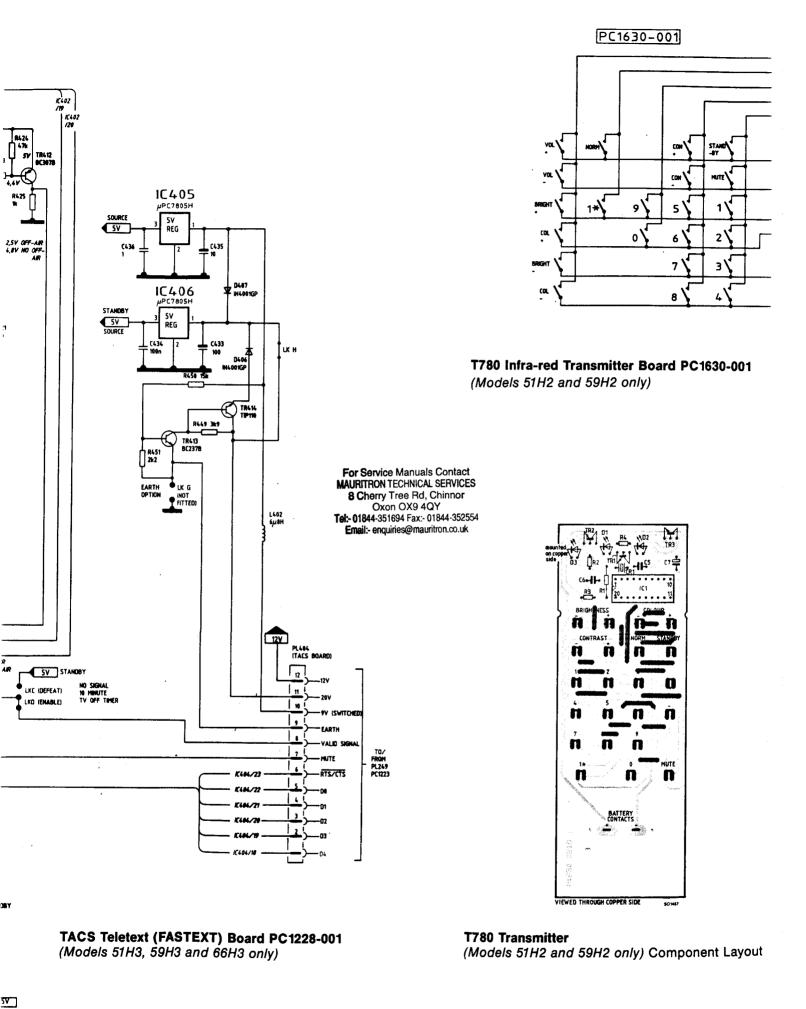




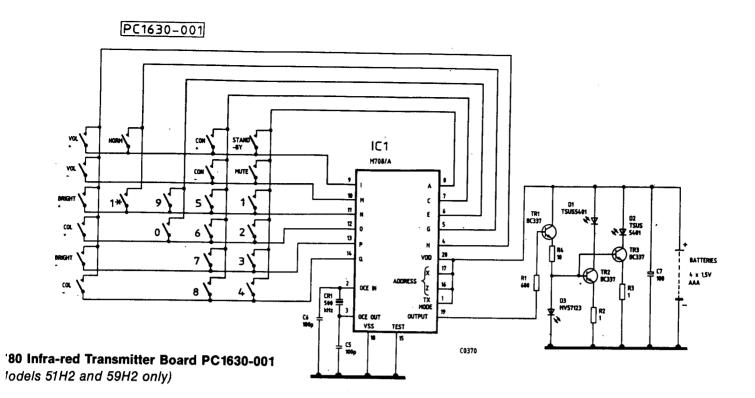
Channel Display Board PC1649-001 (Fitted on all models) Component Layout

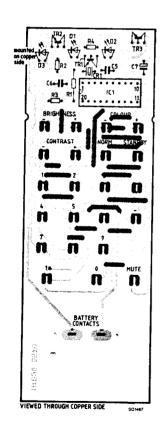


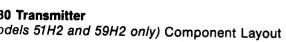


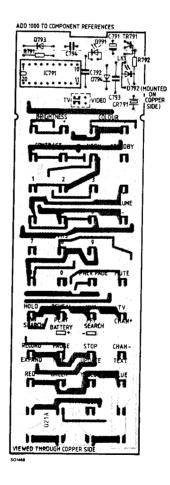


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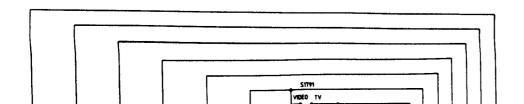


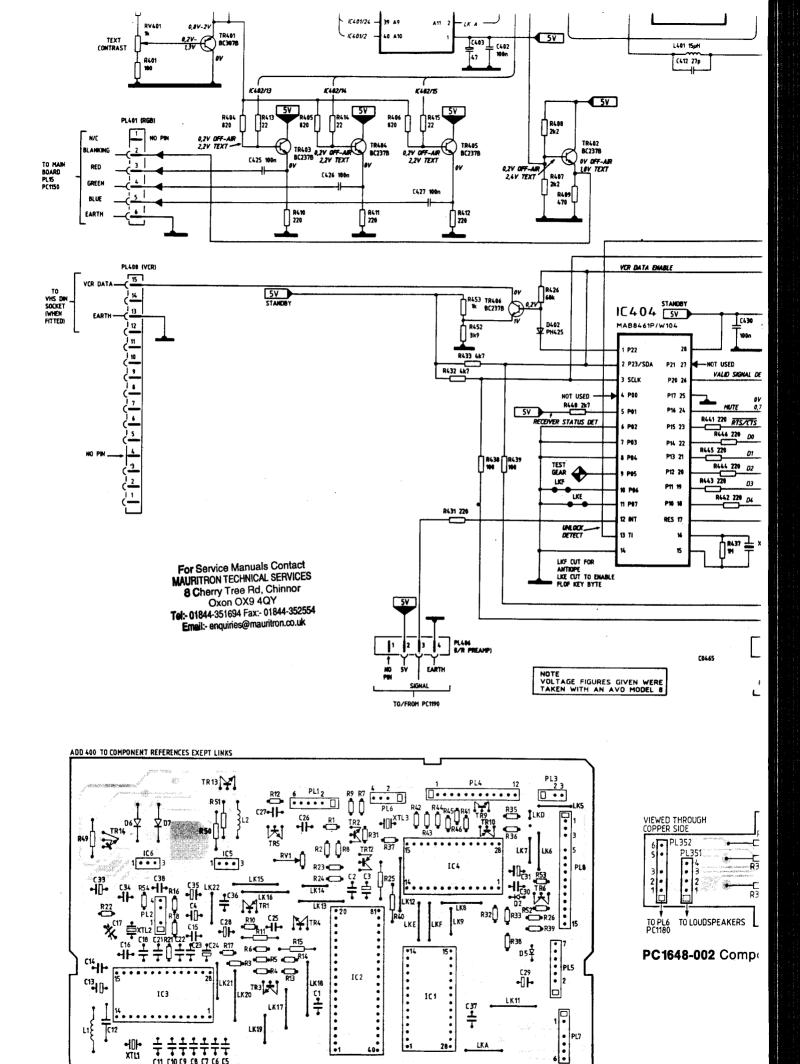






T785 Transmitter (Models 51H3, 59H3 and 66H3 only) Component Layout

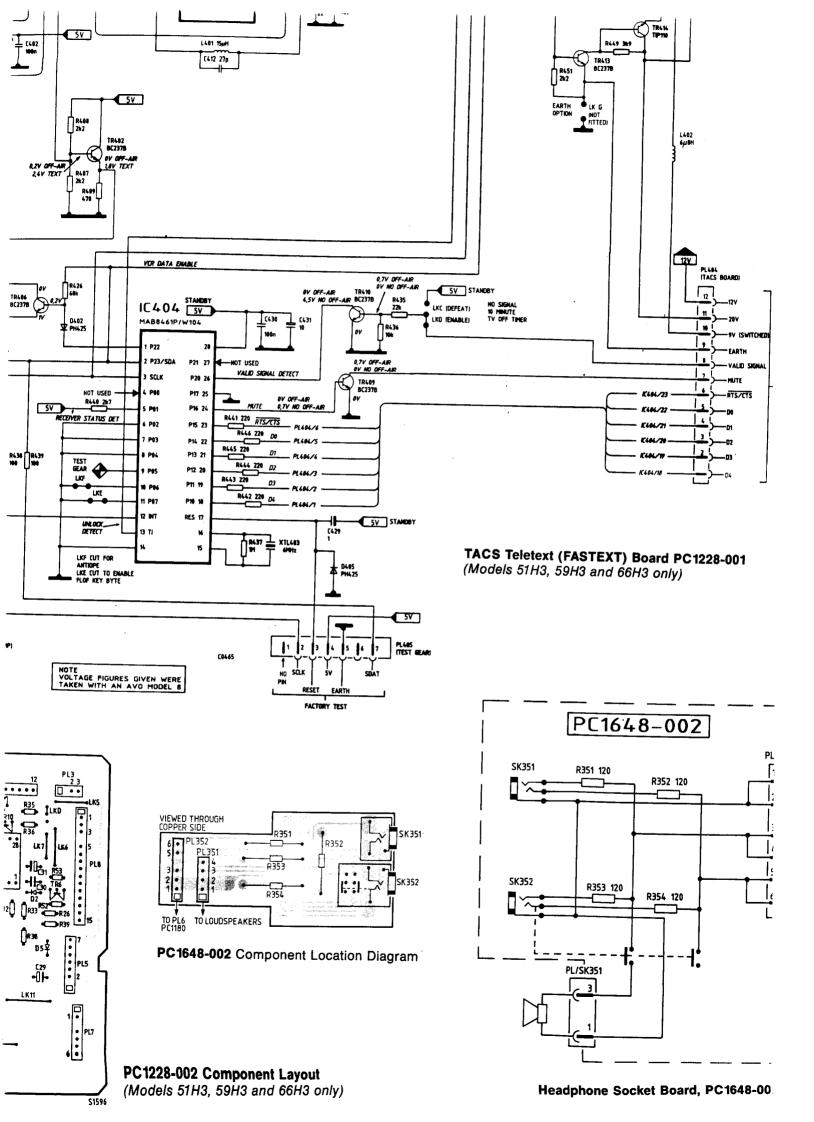


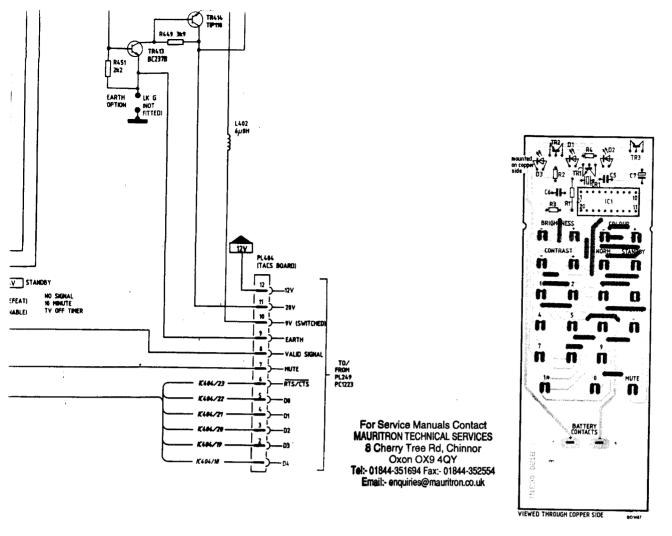


PC1228-002 Component (Models 51H3, 59H3 and

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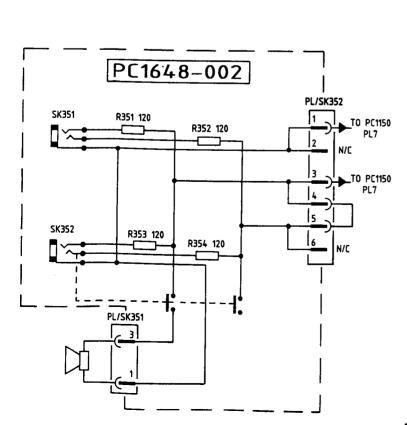
VIEWED THROUGH COPPER SIDE



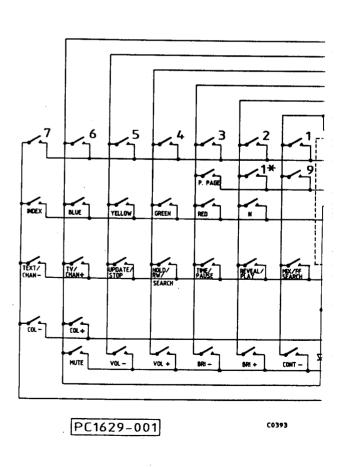


TACS Teletext (FASTEXT) Board PC1228-001 (Models 51H3, 59H3 and 66H3 only)

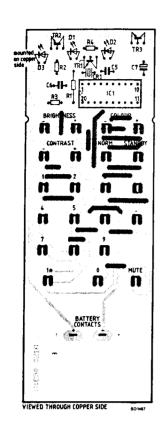
T780 Transmitter (Models 51H2 and 59H2 only) Component Layout



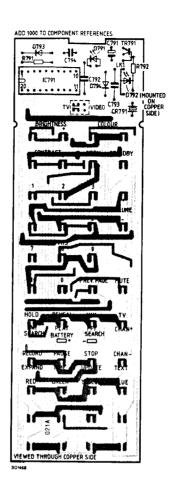
Headphone Socket Board, PC1648-002



T785 Infra-red Transmitter Board PC1629-001 (Models 51H3, 59H3 and 66H3 only)



1 Transmitter dels 51H2 and 59H2 only) Component Layout



T785 Transmitter (Models 51H3, 59H3 and 66H3 only) Component Layout

